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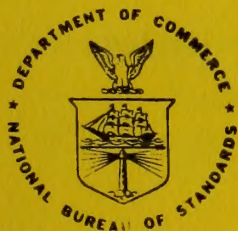
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A New Method of Assigning Uncertainty in Volume Calibration

James A. Lechner, Charles P. Reeve, Clifford H. Spiegelman

Issued December 1980



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James A. Lechner, Charles P. Reeve, Clifford H. Spiegelman

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U.S. DEPARTMENT OF COMMERCE, Philip M. Klutznick, Secretary
Jordan J. Baruch, Assistant Secretary for Productivity, Technology, and Innovation
NATIONAL BUREAU OF STANDARDS, Ernest Ambler, Director

ABSTRACT

*A NEW METHOD OF ASSIGNING UNCERTAINTY IN VOLUME CALIBRATION

by

James A. Lechner
Charles P. Reeve
Clifford H. Spiegelman

with programming assistance from
Martin Ross Cordes and Janice M. Knapp

*Work supported (in part) by the U. S. Nuclear Regulatory Commission.

ABSTRACT

This paper presents a practical statistical overview of the pressure-volume calibration curve for large nuclear materials processing tanks. It explains the appropriateness of applying splines (piecewise polynomials) to this curve, and it presents an overview of the associated statistical uncertainties. In order to implement these procedures a practical and portable FORTRAN IV program is provided along with its users' manual. Finally, the recommended procedure is demonstrated on actual tank data collected by NBS.

Key Words: Volume calibration; differential pressure; splines; accountability; statistics.

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1. Introduction.

The direct measurement of liquid volume in large processing tanks, especially with internal structure, is impractical at best. Measuring (differential) pressure is simple and quick. However, in order to estimate the volume indirectly by observing pressure, it is necessary to use the relationship between volume and pressure. This relationship is known as a calibration curve; its estimation is the process known as calibration.

Fitting a calibration curve is much like regression, in that for "known" values v_i of volume, one obtains one or more observations p_{ij} of the differential pressure $p_i = p(v_i)$, and "fits" a response function $p(v)$ by statistical methods - usually by least squares. At this point, the correspondence stops. Whereas regression is used to predict values of the dependent variable (p) for given values of the independent variable (v), or to test a proposed relationship between the variables, a calibration curve is used to estimate values of the independent variable v corresponding to new measured values of the dependent variable p . Furthermore, the confidence interval (or uncertainty measure) which is desired is not for p , but rather for v . And finally, systematic error is introduced by lack of fit of the calibration curve, and in a materials accounting situation this may be crucial.

This paper presents a method for producing valid uncertainty limits for the pressure-volume tank calibration curve by using calibration functions which are smooth, piecewise polynomial functions called "splines." Taking advantage of an approach to calibration originated by Scheffé [1] and further elucidated by Scheffé, Rosenblatt and

Spiegelman [2], it provides statistically sound uncertainty limits, not just for a single estimated value of volume, but for all volumes estimated by use of the fitted curve. This approach overcomes a major theoretical problem with earlier methods: it makes proper allowance for the contribution to the overall uncertainty of errors in fitting the curve.

The procedure presented herein has been implemented, based upon a spline-fitting program due to deBoor [3]. The resulting FORTRAN program has been tested on various sets of data, including actual tank data.

The remainder of this paper is organized as follows. Section 2 contains a discussion of the pressure-volume model, and the statistics of calibration. Section 3 contains a discussion of an example, and of the printout produced by the program. Section 4 is essentially a users' manual for the program. In Section 5 will be found a discussion of open questions, work in progress, cautions, and possible extensions of this technique. Finally, Appendix 1 contains a discussion of Scheffe's constant c , used as an input to the program, and Appendix 2 contains a listing of the program.

2. The Scientific Basis for, and Interpretation of, a Calibration Curve.

In order to provide statistically valid uncertainty limits for the volume estimates obtained through the use of a calibration curve, it is necessary to have a prior model for the pressure-volume relationship. That is, while the constants in the model for the relationship may be determined from the data, the form of the model must not depend on the data to be used in fitting the relationship. In addition, the less accurately the hypothesized model describes this relationship, the less

valid will be the resulting uncertainty statements. That is, inaccuracies in the hypothesized model will lead to systematic differences between true and fitted curves. In order to obtain valid uncertainty statements, bounds for such differences must be determined, and added to the statistical uncertainty as systematic error limits.

The interiors of large processing tanks do not generally conform to idealized geometrical shapes, such as cylinders. Often, however, the tank can be considered to be composed only of segments for which an idealized model is a good representation. In this paper it is assumed that the tank is composed of a finite number, $k+1$, of distinct and known regions where the idealized relationship between the two variables pressure, p , and volume, v , is given by

$$\begin{aligned}
 p &= f(v) \\
 &= g_1(v) & \xi_0 < v < \xi_1 \\
 &= g_2(v) & \xi_1 < v < \xi_2 \\
 &\vdots \\
 &= g_{k+1}(v) & \xi_k < v < \xi_{k+1} .
 \end{aligned}$$

In addition, continuity of the relationship at the interior "knots" ξ_i , $i=1, \dots, k$ is required.

In all that follows, volume and height refer to the portion of the tank above the bottom of the diptube used to measure pressure. The portion of the tank below that point is known as the heel, and is not treated in this paper. The pressure measured is the difference in

pressure between the bottom of the diptube and a reference point at the top of the tank.

The pressure-volume relationship can be ascertained from the following two equations. At height h the volume in the container is

$$v = \int_0^h A(x) dx$$

where $A(x)$ is the cross-sectional area at height x . Also, when the liquid height is h , $p = h\rho g$, where ρ is the density of the homogeneous liquid and g is the acceleration due to gravity. Using these two equations one easily obtains

$$v = \int_0^{p/\rho g} A(x) dx .$$

Thus $\frac{\partial v}{\partial p} = \frac{1}{\rho g} A(p/\rho g)$ and hence in areas of the tank where $A(x)$ is

constant the volume-pressure relationship is a straight line.

If $A(x)$ is constant* in region i , as it obviously is for at least some regions of the tank shown in Figure 1, then

$$(1) \quad p = g_i(v) = \gamma_i + \beta_i v \text{ for } \xi_{i-1} < v < \xi_i, \quad i=1, \dots, k+1.$$

We assume that each pressure measurement has a random error associated with it, and that these errors are independent and

* If $A(x)$ is not constant on an interval, then p is not a linear function of v on that interval. The program under discussion uses the B-spline basis when higher-order polynomial splines are required, because as pointed out in reference [4], the use of simpler representations of polynomial splines may lead to numerical instability.

normally-distributed, with mean zero and constant variance σ^2 . (Recall that volume is assumed to be measured with no significant error.) Because of these errors, only estimates of the coefficients γ_i and β_i are obtained during the calibration process (experiment). These coefficient estimates are then used during plant operation to obtain estimates of the volume in the tank, utilizing the inverse of the relationship (1).

Determination of uncertainty limits on these estimates is not trivial. There are two sources of random error: estimation of the coefficients γ and β in the calibration experiment, and measurement of p during operational use of the tank. The familiar linear regression model has properties, such as the nonexistence of means and variances of reciprocals, which make the analysis difficult. Special justification involving asymptotic (large sample-size) behavior is thus required in order to use a propagation-of-error approach to obtain appropriate approximate uncertainty limits on the estimated volumes. Furthermore, unless the p - v relationship is linear, normally distributed errors in the p -measurements during operation produce non-normal errors in the resulting estimates of v . The usual propagation-of-error technique does not take into account the differing characteristics of these errors. The new technique presented in this paper, in contrast to the propagation-of-error approach just mentioned, does allow a correct accounting for both.

The calibration chart (i.e., the table of uncertainty limits) is produced after choosing two probabilities, α and δ . An exact statement giving the interpretation of these probabilities may be found in Scheffé

[1] and in Scheffé, Rosenblatt, and Spiegelman [2]. However, an expanded, more heuristic explanation is given here. First, we require bounds for the calibration curve which will contain the entire curve with a prechosen probability $1-\delta$. (Thus, δ can be thought of as describing the uncertainty level to be associated with the outcome of the initial calibration experiment.) These bounds guarantee, with probability $1-\delta$, that for any and every future volume v within the range of calibration of the tank, the v -interval (see Figure 2) that would be obtained by projection of the value $f(v)$ through the curves to \underline{v} and \bar{v} would contain v . The second probability level to be chosen is α . (Here α can be thought of as describing the uncertainty level to be attributed to errors in future individual pressure measurements.) If σ were known, we could state that the true pressure $f(v)$ at the unknown volume v lies within the $1-\alpha$ confidence interval $(p - z_{1-\alpha/2}\sigma, p + z_{1-\alpha/2}\sigma)$ with probability $1-\alpha$, where p is the observed pressure and $z_{1-\alpha/2}$ is the two-sided $1-\alpha$ value for a normal distribution. The Scheffé procedure expands this interval appropriately, to account for the facts that σ is estimated and that this estimate is used for the $1-\delta$ bound on the curve and for bounds on many different $f(v)$. It then combines the $1-\alpha$ confidence interval for $f(v)$ with the $1-\delta$ bounds on the calibration curve to produce calibration intervals $I(p)$ for v . Construction of the calibration intervals is shown schematically in Figure 3. A set of intervals $I(p_i)$ for p_i in the range of values obtained during the calibration experiment is called a calibration chart (see Figure 4).

In the discussion of the example presented in the next section, more detail on the nature of the steps that make up a calibration run will be found.

3. An Example.

This example relates to a processing tank, roughly circular in cross section, but with internal structure consisting of cooling coils, stirrers, braces, etc. [5]. This tank is pictured in Figure 1. The data from calibration runs on this tank have graciously been made available by the author of reference [5].

There were five calibration runs for which the data were useful for this analysis. One run was done in the canyon where the tank is to be used. The other four, done in a mock-up area, used smaller tubing in the pressure-measuring system. This smaller tubing was known to cause systematic differences in the pressure measurement, which were expected to be linearly related to pressure for each run. Since the tubing in the canyon was sufficiently large to render the pressure drop insignificant, the systematic error was estimated for each of the other four runs, and a correction made by applying a linear transformation to the measured pressure. It should be noted that these corrections, made to four of the five runs, effectively decrease the degrees of freedom for the error sum of squares by eight (two correction parameters times four runs corrected).

The calibration program was applied to these data, as were various other techniques available on the large central computer at NBS. The results will now be presented and their use described.

In the version of the program described here, the knot locations are input by the analyst. It is presumed that the knot locations can be adequately prescribed from the blueprints and other knowledge about the tank. (A refinement which allows the automatic determination of the

number and location of knots is being investigated.) The program displays the given knot locations and other input data, as shown in Figure 5. Next come the results of the fitting operation, as shown in part in Figure 6. Note that the fit here is a fit of observed pressure (y) as a function of the accurately-dispensed volume (x); it is pressure which is subject to errors of observation, and volume which is essentially known. The residual standard deviation, an estimate of the standard deviation of the pressure measurements, is derived from the residuals or deviations of the measured pressures from the fitted curve. In this case, its value is 1.49 pascals. This value, the corresponding degrees of freedom, and the coefficients (which are in general not immediately interpretable, since they refer to the so-called B-splines, a representation chosen for computational stability), are part of these results. The calibration intervals for estimation of volume from measured pressure are printed next (see Figure 4). An ordinary polynomial representation and a residual plot are also printed as shown in Figures 7 and 8.

It will be instructive to examine the printout and discuss the approach in more detail, and this will now be done.

As can be seen from Figure 5, the program duplicates the end knots. This is just a simple way to define the B-spline basis functions which are used to perform the fit, and need not concern the analyst. The input values for knot locations, degree of fit, and other miscellaneous parameters are printed out for verification.

At this point, the program does a linear least squares fit of the specified model to the (v,p) data, and prints out a reasonably standard summary (Figure 6). The column labels are self-explanatory. At the bottom of this summary are found the residual standard deviation and its associated degrees of freedom, and the estimated coefficients with the corresponding estimated standard deviations.

The program next computes some intermediate results which generally are of no interest to the analyst, and therefore are only printed out if requested. These are confidence intervals for p, at 300 evenly-spaced points covering the range of v between the extreme knots. Input values of α , δ , and c are used in this procedure, so these values are printed.

The calibration chart comes next, giving the predicted value of v and the corresponding lower and upper limits for each of the specified set of p-values (see Figure 4). It is obtained by inverse interpolation from the confidence intervals for p discussed in the preceding paragraph. Usually, the extreme values of p will be at least partially outside the range of at least one of the curves. When this happens, the intervals should extend either to zero volume or to full volume. This is indicated by "<" and ">" respectively on the printout.

Since the coefficients actually fitted are the B-spline coefficients, the program converts the B-spline representation to a simple polynomial representation. The printout shows the endpoints and the coefficients of the fitted polynomial for each of the specified intervals (see Fig. 7).

Finally, the residuals from the fitted model are plotted in order of increasing volume to allow a visual check of the adequacy of the chosen model [6] (see Fig. 8).

At NBS, with the aid of the central computer and the OMNITAB system [7], a number of other things were tried which strengthen the conviction that this program does indeed work well. These will now be discussed.

Various subsets of the data were fitted to the same model. No inconsistencies were found.

The sensitivity to position and presence of the different knots was checked. The results were rather sensitive to the knot locations, which implies that good estimates of the locations are required for good fits. It should also be noted that where a knot bounds a short segment, the removal of that knot might make very little difference in any global measure of fit quality, unless there are many data points in that short stretch. Nevertheless, the systematic error introduced by deleting that knot can be a consistent source of inventory losses or gains, apparent or real. Thus it is important to include all real segments in the model to be fitted.

A separate program was written to perform linear spline fitting, while the main package was being put together. The answers did not differ between the two programs, providing a partial check that no programming errors were committed.

Smooth higher-order spline fits were tried (quadratic and cubic). There was no improvement in fit. The linear spline appears to provide an adequate representation of the pressure/volume relationship.

Probability plots were done in various ways, looking for possible troubles with the data or the method. Nothing suspicious was found.

4. User's Manual.

This fixed-knot spline package for calibration consists of a "main" subroutine SPLEEN and 29 additional subroutines. The manner in which they interact is diagrammed in Figure 9. All programs are written in FORTRAN and have been checked for portability by the Bell Laboratories PFORT verifier [8]. It was decided that SPLEEN should be a subroutine rather than a main program so that the user could enter the parameter values in the way most convenient for him. The user then must write a main program which sets up the required dimensioned variables and assigns values to the necessary parameters (those with asterisks in the list which follows). These parameters are passed to subroutine SPLEEN via the statement

```
CALL SPLEEN(H,X,Y,W,R1,R2,RES,N,NX,NKX,T,BCOEF,XXI,Q,DIAG,K,  
            KX,YY,NY,NYX,MD,SCRTCH,JX,AL,DL,C,IP)
```

where

- * H(80) = Up to 80 characters in 80A1 format identifying the data
- * X(NX) = Vector (length N) of X-values where observations were made (independent variable)
- * Y(NX) = Vector (length N) of observations
- * W(NX) = Vector (length N) of weights for observations
- R1(NKX) = Vector (length N+K) for scratch area
- R2(NKX) = Vector (length N+K) for scratch area
- RES(NKX) = Vector (length N+K) of residuals from spline fit
- * N = Number of observations
- * NX = Dimension ($>N$) of vectors X,Y,W
- * NKX = Dimension ($>N+K$) of vectors R1,R2,RES
- * T(KX) = Vector (length $K+2*MD$) of knot locations

BCOEF(KX) = Vector (length $K+MD-1$) of B-spline coefficients

XXI(KX,KX) = Variance-covariance matrix (size $[K+MD-1] \times [K+MD-1]$) of B-spline coefficients

Q(JX,KX) = Matrix (size $[MD+1] \times [K+MD-1]$) for scratch area

DIAG(KX) = Vector (length $K+MD-1$) for scratch area

* K = Number of knots specified by user (later increased to $K+2*MD$ by program)

* KX = Dimension ($>K+2*MD$) of vectors T,BCOEF,DIAG and matrices XXI and Q (column only for Q)

* YY(NYX) = Vector (length NY) of Y-values for which predicted X-values (with confidence intervals) are to be computed

* NY = Number of Y-values for which predicted X-values are to be computed

* NYX = Dimension ($>NY$) of vector YY

* MD = Degree of spline (≤ 19); for example, 1=linear, 2=quadratic, 3=cubic)

SCRTCH(JX,JX) = Matrix (size $[MD+1] \times [MD+1]$) for scratch area

* JX = Dimension of square matrix SCRTCH and row dimension of matrix Q = 20

* AL = Alpha level of significance

* DL = Delta level of significance

* C = Constant in the interval (0.85,1.25) associated with Scheffé's calibration technique (see Appendix 1 for a discussion of this constant)

0 For abbreviated printout

* IP = 1 For full printout (residuals, PP representation)

2 For full printout plus Y-confidence intervals for 300 evenly spaced X-values over knot span

Variables which appear with an asterisk (*) require input values from the main program. The subscripts on vectors and matrices indicate the dimensions which must be assigned in the main program.

Variable names which begin with the letters I,J,K,L,M, or N are of the INTEGER type. The remaining variable names are of the REAL single precision type.

The print parameter IP gives the user a certain amount of control over the amount of information to be printed out. Normally the most suitable value is IP=1. A value of IP=0 suppresses the printout of the weights, independent variable, observations, predicted values, and residuals. This option may save quite a bit of paper in case there are several hundred observations, but it deprives the user of the chance to visually examine the residuals. A value of IP=2 causes a listing of certain intermediate vectors which are somewhat lengthy and would not normally be of use to the user.

In the interest of minimizing the number of variables needed in the CALL statement, not all of the printed information can be recovered through the passed parameters. Furthermore, three of the variables (X, K, and T) return values different from their input values.

The data points (X_i, Y_i, W_i) may be input in arbitrary order, as may the knot locations T_i and the vector of YY_i specifying the y-values on the calibration chart.

There are two subroutines which check for consistency among the input parameters. Each inconsistency causes a diagnostic message to be printed. If one or more inconsistencies is detected then the program execution is terminated. Observations outside the knot span are flagged and weighted zero. The number of observations is then reduced by one for each flagged point and a diagnostic is printed. This is not a fatal error unless it reduces the number of degrees of freedom to zero or less.

Although this package can handle splines of any degree up to 19 it was primarily intended for splines of lower degree, i.e., linear, quadratic, or cubic. Test runs on sets of both real and artificial data have given valid results up to about degree 9. Beyond that the limitation of single precision arithmetic on the 36-bit NBS central computer begins to cause roundoff errors that invalidate the results. The user should exercise caution when fitting the higher degree splines.

If the user wants to change some of the continuity conditions at a given knot he may do so by duplicating that knot in the knot vector which is passed to subroutine SPLEEN. If a knot appears M times in the fitting of a spline of degree N then the functional value and the first $N-M$ derivatives of the function will be continuous at that knot. If $M = N+1$, neither the function nor its derivatives are required to be continuous.

The package may be applied to both monotone increasing and decreasing calibration curves.

5. Summary and Discussion.

An approach to calibration curves and their uncertainty bands has been presented, complete with a FORTRAN program to perform the required calculations. An example involving a large process tank has been used to illustrate the approach and the program. The results include not only the curve for estimating volume from measured pressure, but also valid uncertainty limits for repeated applications of the calibration curve obtained.

The interval estimates of volume comprise two parts: a long-term component which changes only at recalibration, and a random component.

The contribution due to the long-term component may be estimated in large scale calibration experiments by the volume interval estimate obtained when $\alpha=1$. Similarly, the contribution due to the random component may be estimated by the volume interval estimate obtained when $\delta=1$. When the calibration experiment is of a more modest size involving less than 100 data points the above component estimates may not be realistic. However a more comprehensive treatment for combining interval estimates (and hence their components) obtained from a calibration curve is under development by C. Spiegelman and K. Eberhardt [9].

The results of a calibration will be used repeatedly, usually without any further opportunity to verify their correctness, until the next calibration. Therefore it is important that the measurement system be under control. In the work reported here, the run-to-run differences observed in the mock-up area were due to a known source (the small diameter of the tubing), and could be corrected. If any anomalous behavior is observed which cannot be satisfactorily explained, then of course the entire statistical analysis must be approached with caution.

Little has been written about the design of calibration experiments - i.e., the selection of volumes at which pressure is to be measured, the number of measurements to be taken at each volume, and the arrangement of these measurement points into a sequence of runs. One solution to this question has been achieved by Spiegelman and Studden, and will be published in the NBS Journal of Research [10]. In general, later runs will concentrate on certain sections of a tank, but it is good practice to ensure that at least two runs cover each section, and that several runs cover the whole tank. If this precaution is not taken, there might

be very little cross-validation between runs.

Certain caveats ought to be mentioned here. The program under discussion assumes that the knot locations are known, and that the model is correct. Consequences of failure of these assumptions could be severe. With respect to the knot locations, careful inspection of the residual plots will sometimes indicate discrepancies. These may be small; however, it is important to realize that such regions represent systematic deviations, and could be used (at least in theory) to cover the diversion of material. An approach to the problem involving unknown knot locations is being pursued at this writing.

Unlike a simple linear regression, where the inclusion of a superfluous higher-order term generally causes no major trouble (the fitted coefficient turns out insignificantly small, and the residual mean square increases minimally), choosing a higher-order model when fitting smooth splines can result in a very much worse fit. This is because of the smoothing restrictions, which greatly limit the freedom of the fitting procedure. (Imagine that the true model consists of two straight lines meeting at a point. If one chooses to fit a quadratic spline, then one is insisting on having two quadratic curves which meet at the proper x-value, and which have the same slope at that point. Thus the slope at that point is probably going to be some value between the two straight-line slopes, and the fit cannot be accurate.) One way around this difficulty is to fit piecewise polynomials (i.e., do not require smoothness), and investigate the appropriate degree from these fits. However, it is much better to know the situation well enough to choose the correct model from physical considerations.

A technique that the authors have found useful is to run the program described here with the degree of the fit set equal to zero. The result is to fit a step function to the data, and to produce a plot of the residuals from that fit; for the Example of this paper, that plot is reproduced as Figure 10. It can be seen that the residuals look as linear as a printer plot can look. Therefore, a first-degree (linear) spline fit is the proper choice. If in some segment the relationship were not linear, this plot should show it. The plot also gives some idea of the spread of points across the intervals, though of course near-duplicate points will plot as one because it is a discrete printer plot.

Note that the continuity restrictions can be relaxed when using the program under consideration, by simply duplicating the knots. See Section 4 for details.

Appendix 1.

As stated in Section 4, a constant c must be input by the user. In order to obtain this constant from tables 1 and 2 in Scheffé (1973) for $1 \leq k \leq 10$ the user must have calculated the standard deviation, SD , for $\hat{p}(v)$ in the complete region of calibration. The smallest and largest values of the $SD(\hat{p}(v))/\hat{\sigma}$ over the complete calibration region are used as input for the Scheffé tables. For $k > 10$ Scheffé gives a mathematical algorithm for finding c , and states that for very large (asymptotic) values of $n-k$, $c=1$. (Here n is the number of observations, and k is the number of B-spline coefficients.) If the reader does not wish to do a Scheffé table 1 or table 2 lookup, the following table gives approximate and generally larger values for this constant.

Approximate c values
for $1 \leq k \leq 10$

$n-k$	60-119	120-149	150 +
c	1.10	1.05	1.00

Appendix 2.

Program Listing.

The subroutines which make up the spline-fitting package follow, in alphabetical order.

```

CPR*NS(1).ADKNTS(2)
1 SUBROUTINE ADKNTS (T,K,KX,MO)
2
3 C-----
4 C ADKNTS WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
5 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
6 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
7 C FOR: DUPLICATING THE FIRST AND KTH (LAST) ENTRIES OF THE KNOT
8 C VECTOR T (MO-1) TIMES
9 C SUBPROGRAMS CALLED: -NONE-
10 C CURRENT VERSION COMPLETED OCTOBER 10, 1979
11 C-----
12 DIMENSION T(KX)
13 10 FORMAT (//1X,29(1H-)/1X,29H* SUMMARY OF KNOT LOCATIONS */1X,
14 20 2 29(1H-)//5X,1H1,6X,8HKNOTS(1)/)
15 30 FORMAT (2X,14,G15.6)
16 30 FORMAT (/5X,30H<<<< EACH END KNOT DUPLICATED,13,1X,
17 2 11H TIMES >>>>)
18 C--- SAVE END KNOT LOCATIONS
19 Q1=T(1)
20 Q2=T(K)
21 C--- INCREASE INDEX OF EACH KNOT LOCATION BY (MO-1)
22 KM=K+MO
23 DO 40 I=1,K
24 KMI=KM-I
25 KI=K-I+1
26 T(KMI)=T(KI)
27 40 CONTINUE
28 C--- ADD DUPLICATE END KNOT LOCATIONS AT THEIR RESPECTIVE ENDS
29 MD=MO-1
30 DO 50 I=1,MD
31 KMI=KM+I-1
32 T(I)=Q1
33 T(KMI)=Q2
34 50 CONTINUE
35 C--- RECOMPUTE THE LENGTH OF THE VECTOR T
36 K=K+2*MD
37 WRITE (6,30) MD
38 WRITE (6,10)
39 DO 60 I=1,K
40 WRITE (6,20) I,T(I)
41 60 CONTINUE
42 RETURN
43 END
ADKNTS01
ADKNTS02
ADKNTS03
ADKNTS04
ADKNTS05
ADKNTS06
ADKNTS07
ADKNTS08
ADKNTS09
ADKNTS10
ADKNTS11
ADKNTS12
ADKNTS13
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ADKNTS40
ADKNTS41
ADKNTS42
ADKNTS43

```

```

CPR*NS(1).BCHFAC(2)
1  SUBROUTINE BCHFAC (W,NBNDMX,NBANDS,NROW,DIAG)
2  C FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3  C CONSTRUCTS CHOLESKY FACTORIZATION
4  C C = L * D * L-TRANSPOSE
5  C WITH L UNIT LOWER TRIANGULAR AND D DIAGONAL, FOR GIVEN MATRIX C OF
6  C ORDER NROW, IN CASE C IS (SYMMETRIC) POSITIVE SEMIDEFINITE
7  C AND Banded, HAVING NBANDS DIAGONALS AT AND BELOW THE
8  C MAIN DIAGONAL.
9
10 C***** INPUT *****
11 C NROW..... IS THE ORDER OF THE MATRIX C .
12 C NBNDMX.... THE ACTUAL ROW DIMENSION OF W.
13 C NBANDS.... INDICATES ITS BANDWIDTH, I.E.,
14 C C(I,J) = 0 FOR ABS(I-J) .GT. NBANDS .
15 C W..... WORKARRAY OF SIZE (NBANDS,NROW) CONTAINING THE NBANDS DIAGO-
16 C NALS IN ITS ROWS, WITH THE MAIN DIAGONAL IN ROW 1 . PRECISELY, BCHFAC16
17 C W(I,J) CONTAINS C(I+J-1,J), I=1,....,NBANDS, J=1,....,NROW. BCHFAC17
18 C FOR EXAMPLE, THE INTERESTING ENTRIES OF A SEVEN DIAGONAL SYM-
19 C METRIC MATRIX C OF ORDER 9 WOULD BE STORED IN W AS
20 C
21 C      11 22 33 44 55 66 77 88 99
22 C      21 32 43 54 65 76 87 98
23 C      31 42 53 64 75 86 97
24 C      41 52 63 74 85 96
25 C
26 C ALL OTHER ENTRIES OF W NOT IDENTIFIED IN THIS WAY WITH AN EN-
27 C TRY OF C ARE NEVER REFERENCED .
28 C DIAG..... IS A WORK ARRAY OF LENGTH NROW .
29 C
30 C***** OUTPUT *****
31 C W.....CONTAINS THE CHOLESKY FACTORIZATION C = L*D*L-TRANSP, WITH
32 C W(1,1) CONTAINING 1/D(1,1)
33 C AND W(I,J) CONTAINING L(I-1+J,J), I=2,....,NBANDS.
34 C
35 C***** METHOD *****
36 C GAUSS ELIMINATION, ADAPTED TO THE SYMMETRY AND BANDEDNESS OF C ,
37 C USED .
38 C NEAR ZERO PIVOTS ARE HANDLED IN A SPECIAL WAY. THE DIAGONAL ELE-
39 C MENT C(N,N) = W(1,N) IS SAVED INITIALLY IN DIAG(N), ALL N. AT THE N-BCHFAC39
40 C TH ELIMINATION STEP, THE CURRENT PIVOT ELEMENT, VIZ. W(1,N), IS COM-
41 C PARED WITH ITS ORIGINAL VALUE, DIAG(N) . IF, AS THE RESULT OF PRIOR
42 C ELIMINATION STEPS, THIS ELEMENT HAS BEEN REDUCED BY ABOUT A WORD
43 C LENGTH, (I.E., IF W(1,N)+DIAG(N) .LE. DIAG(N)), THEN THE PIVOT IS DE-
44 C CLARED TO BE ZERO, AND THE ENTIRE N-TH ROW IS DECLARED TO BE LINEARLY-
45 C DEPENDENT ON THE PRECEDING ROWS. THIS HAS THE EFFECT OF PRODUCING
46 C X(N) = 0 WHEN SOLVING C*X = B FOR X, REGARDLESS OF B. JUSTIFIC-
47 C ATION FOR THIS IS AS FOLLOWS. IN CONTEMPLATED APPLICATIONS OF THIS
48 C PROGRAM, THE GIVEN EQUATIONS ARE THE NORMAL EQUATIONS FOR SOME LEAST-
49 C SQUARES APPROXIMATION PROBLEM, DIAG(N) = C(N,N) GIVES THE NORM-SQUARE
50 C OF THE N-TH BASIS FUNCTION, AND, AT THIS POINT, W(1,N) CONTAINS THE
51 C NORM-SQUARE OF THE ERROR IN THE LEAST-SQUARES APPROXIMATION TO THE N-
52 C TH BASIS FUNCTION BY LINEAR COMBINATIONS OF THE FIRST N-1 . HAVING
53 C W(1,N)+DIAG(N) .LE. DIAG(N) SIGNIFIES THAT THE N-TH FUNCTION IS LIN-
54 C EARLY DEPENDENT TO MACHINE ACCURACY ON THE FIRST N-1 FUNCTIONS, THERE-
55 C FORE CAN SAFELY BE LEFT OUT FROM THE BASIS OF APPROXIMATING FUNCTIONS
56 C THE SOLUTION OF A LINEAR SYSTEM
57 C C*X = B

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58	C	IS EFFECTED BY THE SUCCESSION OF THE FOLLOWING T W O CALLS:	BCHFAC58
59	C	CALL BCFAC (W, NBNDMX, NBANDS, NROW, DIAG) ; TO GET FACTORIZATION	BCHFAC59
60	C	CALL BCSLV (W, NBNDMX, NBANDS, NROW, DIAG) ; TO SOLVE FOR X.	BCHFAC60
61	C	THE VECTOR B NOW CONTAINS X.	BCHFAC61
62	C		BCHFAC62
63	C	MODIFICATION BY.	BCHFAC63
64	C		BCHFAC64
65	C	MARTIN CORDES	BCHFAC65
66	C	CENTER FOR APPLIED MATHEMATICS, NBS	BCHFAC66
67	C	VERSION 1	BCHFAC67
68	C	OCT 1979	BCHFAC68
69	C		BCHFAC69
70	C		BCHFAC70
71	C	INTEGER NBNDMX, NBANDS, NROW, I, IMAX, J, JMAX, N	BCHFAC71
72	C	REAL W(NBNDMX, NROW), DIAG(NROW), RATIO	BCHFAC72
73	C	IF (NROW.GT.1) GO TO 10	BCHFAC73
74	C	IF (W(1,1).GT.0.) W(1,1)=1./W(1,1)	BCHFAC74
75	C	RETURN	BCHFAC75
76	C		BCHFAC76
77	C	DO 20 N=1,NROW	BCHFAC77
78	C	DIAG(N)=W(1,N)	BCHFAC78
79	C		BCHFAC79
80	C	DO 70 N=1,NROW	BCHFAC80
81	C	IF (W(1,N)+DIAG(N).GT.DIAG(N)) GO TO 40	BCHFAC81
82	C	DO 30 J=1,NBANDS	BCHFAC82
83	C	W(J,N)=0.	BCHFAC83
84	C	GO TO 70	BCHFAC84
85	C	W(1,N)=1./W(1,N)	BCHFAC85
86	C	IMAX=MIN0(NBANDS-1,NROW-N)	BCHFAC86
87	C	IF (IMAX.LT.1) GO TO 70	BCHFAC87
88	C	JMAX=IMAX	BCHFAC88
89	C	DO 60 I=1,IMAX	BCHFAC89
90	C	RATIO=W(I+1,N)*W(1,N)	BCHFAC90
91	C	DO 50 J=1,JMAX	BCHFAC91
92	C	L1=N+I	BCHFAC92
93	C	L2=J+I	BCHFAC93
94	C	W(J,L1)=W(J,L1)-W(L2,N)*RATIO	BCHFAC94
95	C	JMAX=JMAX-I	BCHFAC95
96	C	W(I+1,N)=RATIO	BCHFAC96
97	C	CONTINUE	BCHFAC97
98	C	RETURN	BCHFAC98
99	C	END	BCHFAC99

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CPR*NS(1).BCHSLV(1)
1 SUBROUTINE BCHSLV (W,NBNDMX,NBANDS,NROW,B)
2 FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3 SOLVES THE LINEAR SYSTEM C*X = B OF ORDER N R O W FOR X
4 PROVIDED W CONTAINS THE CHOLESKY FACTORIZATION FOR THE BANDED (SYM-BCHSLV03
5 METRIC) POSITIVE DEFINITE MATRIX C AS CONSTRUCTED IN THE SUBROUTINEBCHSLV04
6 B C H F A C (QUO VIDE).
7
8 C***** I N P U T *****
9 C NROW....IS THE ORDER OF THE MATRIX C .
10 C NBNDMX....THE ACTUAL ROW DIMENSION OF W.
11 C NBANDS....INDICATES THE BANDWIDTH OF C .
12 C W....CONTAINS THE CHOLESKY FACTORIZATION FOR C , AS OUTPUT FROM
13 C SUBROUTINE BCFAC (QUO VIDE).
14 C B....THE VECTOR OF LENGTH N R O W CONTAINING THE RIGHT SIDE.
15
16 C***** O U T P U T *****
17 C B....THE VECTOR OF LENGTH N R O W CONTAINING THE SOLUTION.
18
19 C***** M E T H O D *****
20 C WITH THE FACTORIZATION C = L*D*L-TRANSPOSE AVAILABLE, WHERE L IS
21 C UNIT LOWER TRIANGULAR AND D IS DIAGONAL, THE TRIANGULAR SYSTEM
22 C L*Y = B IS SOLVED FOR Y (FORWARD SUBSTITUTION), Y IS STORED IN B,
23 C THE VECTOR D**(-1)*Y IS COMPUTED AND STORED IN B, THEN THE TRIANG-
24 C ULAR SYSTEM L-TRANSPOSE*X = D**(-1)*Y IS SOLVED FOR X (BACKSUBSTIT-
25 C UTION).
26
27 C MODIFICATION BY.
28
29 C MARTIN CORDES
30 C CENTER FOR APPLIED MATHEMATICS, NBS
31 C VERSION 1
32 C OCT 1979
33
34 C-----
35
36 C INTEGER NBNDMX,NBANDS,NROW,J,JMAX,N,NBNDM1
37 C REAL W(NBNDMX,NROW),B(NROW)
38 C IF (NROW.GT.1) GO TO 10
39 C B(1)=B(1)*W(1,1)
40 C RETURN
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42 C
43 C
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BCHSLV58
BCHSLV59
BCHSLV60
BCHSLV61
BCHSLV62
BCHSLV63

L=J+N
B(N)=B(N)-W(J+1,N)*B(L)
N=N-1
IF (N.GT.0) GO TO 40
RETURN
END

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60

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1 SUBROUTINE BSPLPP (T,BCOEF,N,K,SCRATCH,BREAK,COEF,L,KMX)
2 FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3 CALLS BSPLVB
4
5 CONVERTS THE B-REPRESENTATION T, BCOEF, N, K OF SOME SPLINE INTO ITS
6 PP-REPRESENTATION BREAK, COEF, L, K.
7
8 C***** I N P U T *****
9 C T.....KNOT SEQUENCE, OF LENGTH N+K
10 C BCOEF.....B-SPLINE COEFFICIENT SEQUENCE, OF LENGTH N
11 C N.....LENGTH OF BCOEF AND DIMENSION OF SPLINE SPACE
12 C K.....ORDER OF THE SPLINE
13 C KMX.....ROW DIMENSION OF ARRAYS COEF AND SCRATCH
14
15 C W A R N I N G . . . THE RESTRICTION K .LE. KMAX (= 20) IS IMPO-BSPLP001
16 SED BY THE ARBITRARY DIMENSION STATEMENT FOR BIATX BELOW, BUTBSPLP016
17 IS N O W H E R E C H E C K E D FOR.
18
19 C***** W O R K A R E A *****
20 C SCRATCH.....OF SIZE (KMX,K), NEEDED TO CONTAIN BCOEFS OF A PIECE
21 OF THE SPLINE AND ITS K-1 DERIVATIVES
22
23 C***** O U T P U T *****
24 C BREAK.....BREAKPOINT SEQUENCE, OF LENGTH L+1, CONTAINS (IN INCREAS-BSPLP023
25 ING ORDER) THE DISTINCT POINTS IN THE SEQUENCE T(KO,...,T(N+1))BSPLP025
26 C COEF.....ARRAY OF SIZE (KMX,N), WITH COEF(I,J) = (I-1)ST DERIVATIVEBSPLP026
27 OF SPLINE AT BREAK(J) FROM THE RIGHT
28 C L.....NUMBER OF POLYNOMIAL PIECES WHICH MAKE UP THE SPLINE IN THE IN-BSPLP028
29 Terval (T(KO), T(N+1))
30
31 C***** M E T H O D *****
32 C FOR EACH BREAKPOINT INTERVAL, THE K RELEVANT B-COEFS OF THEBSPLP031
33 SPLINE ARE FOUND AND THEN DIFFERENCED REPEATEDLY TO GET THE B-COEFSBSPLP032
34 OF ALL THE DERIVATIVES OF THE SPLINE ON THAT INTERVAL. THE SPLINE ANDBSPLP034
35 ITS FIRST K-1 DERIVATIVES ARE THEN EVALUATED AT THE LEFT END POINTBSPLP035
36 OF THAT INTERVAL, USING BSPLVB REPEATEDLY TO OBTAIN THE VALUES OFBSPLP036
37 ALL B-SPLINES OF THE APPROPRIATE ORDER AT THAT POINT.
38
39 C PARAMETER KMAX = 20
40
41 C MODIFICATION BY.
42
43 C MARTIN CORDES
44 C CENTER FOR APPLIED MATHEMATICS, NBS
45 C VERSION 1
46 C MAR 1980
47
48 C-----
49 C INTEGER K,L,N,I,J,JP1,KMJ,LEFT,LSOFAR
50 C REAL BCOEF(N),BREAK(1),COEF(KMX,1),T(1),SCRATCH(KMX,K),BIATX(20),BSPLP049
51 2 DIFF,FKMJ,SUMBSPLP050
52 C *BIATX(KMAX),DIFF,FKMJ,SUMBSPLP052
53 C DIMENSION BREAK(L+1),COEF(K,L),T(N+K)BSPLP053
54 C CURRENT FORTRAN STANDARD MAKES IT IMPOSSIBLE TO SPECIFY THE LENGTH OFBSPLP054
55 C BREAK, COEF AND T PRECISELY WITHOUT THE INTRODUCTION OF OTHERWISEBSPLP055
56 C SUPERFLUOUS ADDITIONAL ARGUMENTS.
57 C BSPLP057

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58 LSOFAR=0
59 BREAK(1)=T(K)
60 DO 60 LEFT=K,N
61 C
62 IF (T(LEFT+1).EQ.T(LEFT)) GO TO 60
63 LSOFAR=LSOFAR+1
64 BREAK(LSOFAR+1)=T(LEFT+1)
65 IF (K.GT.1) GO TO 10
66 COEF(1,LSOFAR)=BCOEF(LEFT)
67 GO TO 60
68 C
69 STORE THE K B-SPLINE COEFF.S RELEVANT TO CURRENT KNOT INTERVAL
70 IN SCRTCH(.,1) .
71 DO 20 I=1,K
72 M=LEFT-K+1
73 SCRTCH(I,1)=BCOEF(M)
74 C
75 FOR J=1,...,K-1, COMPUTE THE K-J B-SPLINE COEFF.S RELEVANT TOBSPLP074
76 CURRENT KNOT INTERVAL FOR THE J-TH DERIVATIVE BY DIFFERENCING
77 THOSE FOR THE (J-1)ST DERIVATIVE, AND STORE IN SCRTCH(.,J+1) .
78 DO 30 JP1=2,K
79 J=JP1-1
80 KMJ=K-J
81 FKMJ=FLOAT(KMJ)
82 DO 30 I=1,KMJ
83 M1=LEFT+I
84 M2=M1-KMJ
85 DIFF=T(M1)-T(M2)
86 IF (DIFF.GT.0.) SCRTCH(I,JP1)=((SCRTCH(I+1,J)-SCRTCH(I,J))/DIFF)*FBSPLP085
87 2KMJ
88 C
89 CONTINUE
90 C
91 FOR J = 0, ..., K-1, FIND THE VALUES AT T(LEFT) OF THE J+1
92 B-SPLINES OF ORDER J+1 WHOSE SUPPORT CONTAINS THE CURRENT
93 KNOT INTERVAL FROM THOSE OF ORDER J (IN BIATX), THEN COMB-
94 INE WITH THE B-SPLINE COEFF.S (IN SCRTCH(.,K-J)) FOUND EARLIERBSPLP092
95 TO COMPUTE THE (K-J-1)ST DERIVATIVE AT T(LEFT) OF THE GIVEN
96 SPLINE.
97 NOTE. IF THE REPEATED CALLS TO BSPLVB ARE THOUGHT TO GENE-BSPLP095
98 RATE TOO MUCH OVERHEAD, THEN REPLACE THE FIRST CALL BY
99 BIATX(1) = 1.
100 AND THE SUBSEQUENT CALL BY THE STATEMENT
101 J = JP1 - 1
102 DELTAR(J) = T(LEFT+J) - X
103 C
104 .....
105 BIATX(J+1) = SAVED
106 FROM BSPLVB . DELTAR(KMAX) AND DELTAR(KMAX) WOULD HAVE TO
107 APPEAR IN A DIMENSION STATEMENT, OF COURSE.
108 C
109 CALL BSPLVB (T,1,1,T(LEFT),LEFT,BIATX)
110 COEF(K,LSOFAR)=SCRTCH(1,K)
111 DO 50 JP1=2,K
112 CALL BSPLVB (T,JP1,2,T(LEFT),LEFT,BIATX)
113 KMJ=K+1-JP1
114 SUM=0.
115 DO 40 I=1,JP1
116 SUM=BIATX(I)*SCRTCH(I,KMJ)+SUM
117 COEF(KMJ,LSOFAR)=SUM
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BSPLP116
BSPLP117
BSPLP118
BSPLP119

CONTINUE
L=LSOFAR
RETURN
END

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116
117
118
119


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CPR*NS(1).BSPLVB(1)
1 SUBROUTINE BSPLVB (T,JHIGH,INDEX,X,LEFT,BIATX)
2 FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3 CALCULATES THE VALUE OF ALL POSSIBLY NONZERO B-SPLINES AT X OF ORDER
4
5 C JOUT = MAX( JHIGH , (J+1)*(INDEX-1) )
6
7 C WITH KNOT SEQUENCE T.
8
9 C***** I N P U T *****
10 C T.....KNOT SEQUENCE, OF LENGTH LEFT + JOUT , ASSUMED TO BE NONDE-
11 C CRESING. A S U M P T I O N . . . . .
12 C T(LEFT) .LT. T(LEFT + 1)
13 C D I V I S I O N B Y Z E R O WILL RESULT IF T(LEFT) = T(LEFT+1)
14 C JHIGH,
15 C INDEX.....INTEGERS WHICH DETERMINE THE ORDER JOUT = MAX(JHIGH,
16 C (J+1)*(INDEX-1)) OF THE B-SPLINES WHOSE VALUES AT X ARE TO
17 C BE RETURNED. INDEX IS USED TO AVOID RECALCULATIONS WHEN SEVE-
18 C RAL COLUMNS OF THE TRIANGULAR ARRAY OF B-SPLINE VALUES ARE NEE-
19 C DED (E.G., IN BVALUE OR IN BSPLVD ). PRECISELY,
20 C IF INDEX = 1,
21 C THE CALCULATION STARTS FROM SCRATCH AND THE ENTIRE TRIANGULAR
22 C ARRAY OF B-SPLINE VALUES OF ORDERS 1,2,...,JHIGH IS GENERATED
23 C ORDER BY ORDER , I.E., COLUMN BY COLUMN .
24 C IF INDEX = 2,
25 C ONLY THE B-SPLINE VALUES OF ORDER J+1, J+2, ..., JOUT ARE GE-
26 C NERATED, THE ASSUMPTION BEING THAT BIATX, J, DELTAL, DELTARBSPLVB26
27 C ARE, ON ENTRY, AS THEY WERE ON EXIT AT THE PREVIOUS CALL.
28 C IN PARTICULAR, IF JHIGH = 0, THEN JOUT = J+1, I.E., JUST
29 C THE NEXT COLUMN OF B-SPLINE VALUES IS GENERATED.
30 C
31 C W A R N I N G . . . . THE RESTRICTION JOUT.LE. JMAX (= 20) IS IM-
32 C POSED ARBITRARILY BY THE DIMENSION STATEMENT FOR DELTAL AND
33 C DELTAR BELOW, BUT IS N O W H E R E C H E C K E D F O R .
34 C
35 C X.....THE POINT AT WHICH THE B-SPLINES ARE TO BE EVALUATED.
36 C LEFT.....AN INTEGER CHOSEN (USUALLY) SO THAT
37 C T(LEFT) .LE. X .LE. T(LEFT+1) .
38 C
39 C***** O U T P U T *****
40 C BIATX.....ARRAY OF LENGTH JOUT , WITH BIATX(I) CONTAINING THE VAL-
41 C UE AT X OF THE POLYNOMIAL OF ORDER JOUT WHICH AGREES WITH
42 C THE B-SPLINE B(LEFT-JOUT+1,JOUT,T) ON THE INTERVAL (T(LEFT),
43 C T(LEFT+1)) .
44 C
45 C***** M E T H O D *****
46 C THE RECURRENCE RELATION
47 C
48 C 
$$B(I,J+1)(X) = \frac{X - T(I)}{T(I+J) - T(I)} B(I,J)(X) + \frac{T(I+J+1) - X}{T(I+J+1) - T(I+1)} B(I+1,J)(X)$$

49 C
50 C
51 C IS USED (REPEATEDLY) TO GENERATE THE (J+1)-VECTOR B(LEFT-J,J+1)(X),
52 C ...,B(LEFT,J+1)(X) FROM THE J-VECTOR B(LEFT-J+1,J)(X), ...,
53 C B(LEFT,J)(X), STORING THE NEW VALUES IN BIATX OVER THE OLD. THE
54 C FACTS THAT
55 C 
$$B(I,1) = 1 \text{ IF } T(I) .LE. X .LT. T(I+1)$$

56 C AND THAT
57 C

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58 C B(I,J)(X) = 0 UNLESS T(I) .LE. X .LT. T(I+J) BSPLVB58
59 C ARE USED. THE PARTICULAR ORGANIZATION OF THE CALCULATIONS FOLLOWS AL- BSPLVB59
60 C GORITHM (8) IN CHAPTER X OF THE TEXT. BSPLVB60
61 C BSPLVB61
62 C PARAMETER JMAX = 20 BSPLVB62
63 C INTEGER INDEX,JHIGH,LEFT,I,J,JP1 BSPLVB63
64 C REAL BIATX(JHIGH),T(1),X, DELTAL(JMAX),DELTAR(JMAX),SAVED,TERM BSPLVB64
65 C REAL BIATX(JHIGH),T(1),X,DELTAL(20),DELTAR(20),SAVED,TERM BSPLVB65
66 C DIMENSION BIATX(JOUT), T(LEFT+JOUT) BSPLVB66
67 C CURRENT FORTRAN STANDARD MAKES IT IMPOSSIBLE TO SPECIFY THE LENGTH OF BSPLVB67
68 C T AND OF BIATX PRECISELY WITHOUT THE INTRODUCTION OF OTHERWISE BSPLVB68
69 C SUPERFLUOUS ADDITIONAL ARGUMENTS. BSPLVB69
70 C DATA J /1/ BSPLVB70
71 C SAVE J,DELTAL,DELTAR (VALID IN FORTRAN 77) BSPLVB71
72 C BSPLVB72
73 C GO TO (10,20), INDEX BSPLVB73
74 C J=1 BSPLVB74
75 C BIATX(1)=1. BSPLVB75
76 C IF (J.GE.JHIGH) GO TO 40 BSPLVB76
77 C BSPLVB77
78 C JP1=J+1 BSPLVB78
79 C L=LEFT+J BSPLVB79
80 C DELTAR(J)=T(L)-X BSPLVB80
81 C L=LEFT+1-J BSPLVB81
82 C DELTAL(J)=X-T(L) BSPLVB82
83 C SAVED=0. BSPLVB83
84 C DO 30 I=1,J BSPLVB84
85 C L=JP1-I BSPLVB85
86 C TERM=BIATX(I)/(DELTAR(I)+DELTAL(L)) BSPLVB86
87 C BIATX(I)=SAVED+DELTAR(I)*TERM BSPLVB87
88 C SAVED=DELTAL(L)*TERM BSPLVB88
89 C BIATX(JP1)=SAVED BSPLVB89
90 C J=JP1 BSPLVB90
91 C IF (J.LT.JHIGH) GO TO 20 BSPLVB91
92 C BSPLVB92
93 C RETURN BSPLVB93
94 C END BSPLVB94

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CPR*NS(1), BVALUE(2)

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1 REAL FUNCTION BVALUE(T,BCOEF,N,K,X,JDERIV)
2 FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3 CALLS INTERV
4
5 CALCULATES VALUE AT X OF JDERIV-TH DERIVATIVE OF SPLINE FROM B-REPR.
6 THE SPLINE IS TAKEN TO BE CONTINUOUS FROM THE RIGHT.
7
8 C***** I N P U T *****
9 C T, BCOEF, N, K,..... FORMS THE B-REPRESENTATION OF THE SPLINE F TO
10 BE EVALUATED. SPECIFICALLY,
11 T,..... KNOT SEQUENCE, OF LENGTH N+K, ASSUMED NONDECREASING.
12 BCOEF,..... B-COEFFICIENT SEQUENCE, OF LENGTH N.
13 N,..... LENGTH OF BCOEF AND DIMENSION OF SPLINE(K,T),
14 A S S U M E D P O S I T I V E.
15 K,..... ORDER OF THE SPLINE.
16
17 W A R N I N G. . . . THE RESTRICTION K.LE. KMAX (=20) IS IMPOSED
18 ARBITRARILY BY THE DIMENSION STATEMENT FOR AJ, DL, DR BELOW,
19 BUT IS N O W H E R E C H E C K E D F O R.
20
21 X,..... THE POINT AT WHICH TO EVALUATE.
22 JDERIV,..... INTEGER GIVING THE ORDER OF THE DERIVATIVE TO BE EVALUATED
23 A S S U M E D T O B E Z E R O O R P O S I T I V E.
24
25 C***** O U T P U T *****
26 C BVALUE,..... THE VALUE OF THE (JDERIV)-TH DERIVATIVE OF F AT X.
27
28 C***** M E T H O D *****
29 C THE NONTRIVIAL KNOT INTERVAL (T(I),T(I+1)) CONTAINING X IS LO-BVALUE29
30 CATED WITH THE AID OF INTERV. THE K B-COEFFS OF F RELEVANT FOR BVALUE30
31 THIS INTERVAL ARE THEN OBTAINED FROM BCOEF (OR TAKEN TO BE ZERO IF
32 NOT EXPLICITLY AVAILABLE) AND ARE THEN DIFFERENCED JDERIV TIMES TO
33 OBTAIN THE B-COEFFS OF (D**JDERIV)F RELEVANT FOR THAT INTERVAL.
34 PRECISELY, WITH J = JDERIV, WE HAVE FROM X.(12) OF THE TEXT THAT
35
36 (D**J)F = SUM ( BCOEF(.,J)*B(.,K-J,T) )
37
38 WHERE
39 / BCOEF(.,J) , J.EQ. 0
40 / BCOEF(.,J-1) - BCOEF(.,-1,J-1)
41 / ----- , J.GT. 0
42 / (T(.,K-J) - T(.,J-1))/(K-J)
43
44 THEN, WE USE REPEATEDLY THE FACT THAT
45
46 SUM ( A(.,M)*B(.,M,T)(X) ) = SUM ( A(.,X)*B(.,M-1,T)(X) )
47 WITH
48 (X - T(.,J))*A(.,J) + (T(.,M-1) - X)*A(.,-1)
49 A(.,X) = -----
50 (X - T(.,J)) + (T(.,M-1) - X)
51
52 TO WRITE (D**J)F(X) EVENTUALLY AS A LINEAR COMBINATION OF B-SPLINES
53 OF ORDER 1, AND THE COEFFICIENT FOR B(1,1,T)(X) MUST THEN BE THE
54 DESIRED NUMBER (D**J)F(X). (SEE X.(17)-(19) OF TEXT).
55
56 PARAMETER KMAX = 20
57

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58 INTEGER JDERIV,K,N,I,ILO,IMK,J,JC,JCMIN,JCMAX,JJ,KMJ,KM1,MFLAG,NMIBVALU058
59 2,JDRVPI BVALU059
60 REAL BCOEF(N),T(1),X,AJ(20),DL(20),DR(20),FKMJ BVALU060
61 REAL BCOEF(N),T(1),X, AJ(KMAX),DL(KMAX),DR(KMAX),FKMJ BVALU061
62 DIMENSION T(N+K) BVALU062
63 CURRENT FORTRAN STANDARD MAKES IT IMPOSSIBLE TO SPECIFY THE LENGTH OF TBVALU063
64 C PRECISELY WITHOUT THE INTRODUCTION OF OTHERWISE SUPERFLUOUS ADDITION-BVALU064
65 C AL ARGUMENTS. BVALU065
66 BVALUE=0. BVALU066
67 IF (JDERIV.GE.K) GO TO 170 BVALU067
68 BVALU068
69 *** FIND I S.T. 1.LE. I .LT. N+K AND T(I) .LT. T(I+1) ANDBVALU069
70 T(I) .LE. X .LT. T(I+1) . IF NO SUCH I CAN BE FOUND, X LIES BVALU070
71 OUTSIDE THE SUPPORT OF THE SPLINE F AND BVALUE = 0. BVALU071
72 (THE ASYMMETRY IN THIS CHOICE OF I MAKES F RIGHTCONTINUOUS) BVALU072
73 CALL INTERV (T,N+K,X,I,MFLAG) BVALU073
74 IF (MFLAG.NE.0) GO TO 170 BVALU074
75 *** IF K = 1 (AND JDERIV = 0), BVALUE = BCOEF(I). BVALU075
76 KM1=K-1 BVALU076
77 IF (KM1.GT.0) GO TO 10 BVALU077
78 BVALUE=BCOEF(I) BVALU078
79 GO TO 170 BVALU079
80 C BVALU080
81 C *** STORE THE K B-SPLINE COEFFICIENTS RELEVANT FOR THE KNOT INTERVAL BVALU081
82 (T(I),T(I+1)) IN AJ(1),...,AJ(K) AND COMPUTE DL(J) = X - T(I+1-J), BVALU082
83 DR(J) = T(I+J) - X, J=1,...,K-1 . SET ANY OF THE AJ NOT OBTAINABLE BVALU083
84 FROM INPUT TO ZERO. SET ANY T.S NOT OBTAINABLE EQUAL TO T(1) OR BVALU084
85 TO T(N+K) APPROPRIATELY. BVALU085
86 JCMIN=1 BVALU086
87 IMK=I-K BVALU087
88 IF (IMK.GE.0) GO TO 40 BVALU088
89 JCMIN=1-IMK BVALU089
90 DO 20 J=1,I BVALU090
91 L=I+1-J BVALU091
92 DL(J)=X-T(L) BVALU092
93 DO 30 J=1,KM1 BVALU093
94 L=K-J BVALU094
95 AJ(L)=0. BVALU095
96 DL(J)=DL(I) BVALU096
97 GO TO 60 BVALU097
98 DO 50 J=1,KM1 BVALU098
99 L=I+1-J BVALU099
100 DL(J)=X-T(L) BVALU100
101 C BVALU101
102 JCMAX=K BVALU102
103 NM1=N-I BVALU103
104 IF (NM1.GE.0) GO TO 90 BVALU104
105 JCMAX=K+NM1 BVALU105
106 DO 70 J=1,JCMAX BVALU106
107 L=I+J BVALU107
108 DR(J)=T(L)-X BVALU108
109 DO 80 J=JCMAX,KM1 BVALU109
110 AJ(J+1)=0. BVALU110
111 DR(J)=DR(JCMAX) BVALU111
112 GO TO 110 BVALU112
113 DO 100 J=1,KM1 BVALU113
114 L=I+J BVALU114
115 DR(J)=T(L)-X BVALU115

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116 BVALU116
117 BVALU117
118 BVALU118
119 BVALU119
120 BVALU120
121 BVALU121
122 BVALU122
123 BVALU123
124 BVALU124
125 BVALU125
126 BVALU126
127 BVALU127
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136 BVALU136
137 BVALU137
138 BVALU138
139 BVALU139
140 BVALU140
141 BVALU141
142 BVALU142
143 BVALU143
144 BVALU144

C
110 DO 120 JC=JCMIN,JCMAX
117 L=IMK+JC
120 AJ(JC)=BCOEF(L)
C
120 *** DIFFERENCE THE COEFFICIENTS JDERIV TIMES.
121 IF (JDERIV.EQ.0) GO TO 140
122 DO 130 J=1,JDERIV
123 KMJ=K-J
124 FKMJ=FLOAT(KMJ)
125 ILO=KMJ
126 DO 130 JJ=1,KMJ
127 AJ(JJ)=((AJ(JJ+1)-AJ(JJ))/(DL(ILO)+DR(JJ)))*FKMJ
128 ILO=ILO-1
129
130
131 C *** COMPUTE VALUE AT X IN (T(I),T(I+1)) OF JDERIV-TH DERIVATIVE,
132 GIVEN ITS RELEVANT B-SPLINE COEFFS IN AJ(1),...,AJ(K-JDERIV).
133 IF (JDERIV.EQ.KM1) GO TO 160
134 JDRVPI=JDERIV+1
135 DO 150 J=JDRVPI,KM1
136 KMJ=K-J
137 ILO=KMJ
138 DO 150 JJ=1,KMJ
139 AJ(JJ)=(AJ(JJ+1)*DL(ILO)+AJ(JJ)*DR(JJ))/(DL(ILO)+DR(JJ))
140 ILO=ILO-1
141 BVALUE=AJ(1)
142
143 C
144 RETURN
145 END

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CPR*NS(1).CHECK1(2)
1 SUBROUTINE CHECK1 (W,N,NX,K,KX,NKX,NY,NYX,JX,MO,AL,DL,C,WZ)
2
3 CHECK1 WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4 DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5 AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6 FOR: CHECKING WHETHER INPUT VALUES FALL WITHIN THEIR ALLOWABLE
7 LIMITS
8 SUBPROGRAMS CALLED: -NONE-
9 CURRENT VERSION COMPLETED JUNE 20, 1980
10
11 DIMENSION W(NX)
12 WRITE FORMATS
13 10 FORMAT (/1X,21H*** VECTOR LENGTH N = ,14,2X,20HEXCEEDS DIMENSIONED
14 2,10HVALUE NX = ,14)
15 20 FORMAT (/1X,18H*** DIMENSION KX = ,14,2X,20H MUST BE AT LEAST AS ,
16 2 8HLARGE AS/5X,26HK + 2*(DEGREE OF SPLINE) = ,14)
17 30 FORMAT (/1X,22H*** VECTOR LENGTH NY = ,14,2X,
18 2 20HEXCEEDS DIMENSIONED ,11HVALUE NYX = ,14)
19 40 FORMAT (/1X,17H*** WEIGHT NUMBER,15,1X,13HIS NEGATIVE (,G10.5,1H) )
20 50 FORMAT (/1X,22H*** DEGREE OF SPLINE (,13,12H) EXCEEDS 19)
21 60 FORMAT (/1X,28H*** NUMBER OF OBSERVATIONS (,14,13H) MUST EXCEED,
22 2 15)
23 70 FORMAT (/1X,33H*** ALPHA LEVEL OF SIGNIFICANCE (,F6.3,
24 2 10H) MUST BE ,21HIN THE INTERVAL (0,1))
25 80 FORMAT (/1X,33H*** DELTA LEVEL OF SIGNIFICANCE (,F6.3,
26 2 10H) MUST BE ,21HIN THE INTERVAL (0,1))
27 90 FORMAT (/1X,16H*** CONSTANT C (,F6.3,26H) MUST BE IN THE INTERVAL
28 2,11H0.85,1.25))
29 100 FORMAT (/1X,14,1X,40HERROR CONDITIONS DETECTED BY SUBROUTINE ,
30 2 8H*CHECK1*//6X,38H*****PROGRAM EXECUTION TERMINATED*****//)
31 110 FORMAT (/1X,47H*** MAXIMUM ORDER OF SPLINES JX MUST BE 20 (NOT,13,
32 2 1H) )
33 120 FORMAT (/5X,42HSEE APPENDIX 1 OF THE FOLLOWING NBS PAPER://5X,
34 2 36HA NEW APPROACH TO VOLUME CALIBRATION/5X,
35 3 51HBY J. A. LECHNER, C. P. REEVE, AND C. H. SPIEGELMAN/)
36 130 FORMAT (/1X,23H*** VECTOR LENGTH N+K = ,14,2X,
37 2 20HEXCEEDS DIMENSIONED ,11HVALUE NKX = ,14)
38 C--- INITIALIZE COUNT FOR ERROR CONDITIONS
39 KOUNT=0
40
41 C--- INITIALIZE NUMBER OF ZERO WEIGHTS
42 NZ=0
43
44 C--- CHECK FOR VECTOR LENGTHS EXCEEDING DIMENSIONED VALUES
45 IF (N.LE.NX) GO TO 140
46 KOUNT=KOUNT+1
47 WRITE (6,10) N,NX
48 NK=N+K
49 IF (NK.LE.NKX) GO TO 150
50 KOUNT=KOUNT+1
51 WRITE (6,130) NK,NKX
52 K2=K+2*(MO-1)
53 IF (K2.LE.KX) GO TO 160
54 KOUNT=KOUNT+1
55 WRITE (6,20) KX,K2
56 IF (NY.LE.NYX) GO TO 170
57 KOUNT=KOUNT+1
58 WRITE (6,30) NY,NYX
59 CHECK FOR NEGATIVE AND ZERO WEIGHTS
60

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58	170	DO 200 I=1,N	CHECK158
59		IF (N(I)) 180,190,200	CHECK159
60	C---	COUNT EACH NEGATIVE WEIGHT AS AN ERROR CONDITION	CHECK160
61	180	KOUNT=KOUNT+1	CHECK161
62		WRITE (6,40) I,W(I)	CHECK162
63		GO TO 200	CHECK163
64	C---	COUNT ZERO WEIGHTS	CHECK164
65	190	NZ=NZ+1	CHECK165
66	200	CONTINUE	CHECK166
67	C---	CHECK FOR MAXIMUM ORDER OF SPLINE = 20	CHECK167
68		IF (JX.EQ.20) GO TO 210	CHECK168
69		KOUNT=KOUNT+1	CHECK169
70		WRITE (6,110) JX	CHECK170
71	C---	CHECK ORDER OF SPLINE	CHECK171
72	210	IF (MO.LE.20) GO TO 220	CHECK172
73		KOUNT=KOUNT+1	CHECK173
74		MD=MO-1	CHECK174
75		WRITE (6,50) MD	CHECK175
76	C---	CHECK NUMBER OF OBSERVATIONS	CHECK176
77	220	K2=K+MO-2+NZ	CHECK177
78		IF (N.GT.K2) GO TO 230	CHECK178
79		KOUNT=KOUNT+1	CHECK179
80		WRITE (6,60) N,K2	CHECK180
81	C---	CHECK SIGNIFICANCE LEVELS	CHECK181
82	230	IF (AL.GT.0.0.AND.AL.LE.1.0) GO TO 240	CHECK182
83		KOUNT=KOUNT+1	CHECK183
84		WRITE (6,70) AL	CHECK184
85	240	IF (DL.GT.0.0.AND.DL.LE.1.0) GO TO 250	CHECK185
86		KOUNT=KOUNT+1	CHECK186
87		WRITE (6,80) DL	CHECK187
88	C---	CHECK CONSTANT C	CHECK188
89	250	IF (C.LE.1.25.AND.C.GE.0.85) GO TO 260	CHECK189
90		KOUNT=KOUNT+1	CHECK190
91		WRITE (6,90) C	CHECK191
92		WRITE (6,120)	CHECK192
93	C---	CHECK WHETHER ANY ERROR CONDITIONS EXIST	CHECK193
94	260	IF (KOUNT.EQ.0) RETURN	CHECK194
95		WRITE (6,100) KOUNT	CHECK195
96		STOP	CHECK196
97		END	CHECK197

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CPR*NS(1).CHECK2(1)
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SUBROUTINE CHECK2 (T,K,KX,X,W,N,NX,NZ,MO)
C-----
C CHECK2 WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
C FOR: CHECKING FOR OBSERVATIONS WHICH LIE OUTSIDE THE SEQUENCE OF
C KNOTS. THE WEIGHTS OF SUCH OBSERVATIONS ARE SET TO ZERO.
C SUBPROGRAMS CALLED: -NONE-
C CURRENT VERSION COMPLETED MARCH 24, 1980
C-----
C DIMENSION T(KX),X(NX),W(NX)
C FORMAT (/1X,6H*** X(,14,3H) =,G12.6,1X,22HIS OUTSIDE KNOT SPAN. ,
10 2 1X,11HSET WEIGHT(,14,5H) =0.)
C FORMAT (/1X,48H*** ADDITIONAL ZERO WEIGHTS GIVE NONPOSITIVE ***/9XCHECK214
20 2,32HDEGREES OF FREEDOM FOR RESIDUALS//6X,13H*****PROGRAM ,
C 3 25HEXECUTION TERMINATED*****//)
C FORMAT (/1X,15H*** VALUE OF X(,14,14H) CHANGED FROM,G14.8,2X,2HT0,
30 2 G14.8/5X,45HS0 THAT IT WILL BE LESS THAN THE LARGEST KNOT)
C DO 60 I=1,N
C IF (W(I).EQ.0.0) GO TO 60
C IF (X(I).LT.T(1)) GO TO 50
C IF (X(I)-T(K)) 60,40,50
C XOLD=X(I)
C X(I)=XOLD-ABS(XOLD)*0.0000001
C WRITE (6,30) I,XOLD,X(I)
C GO TO 60
C W(I)=0.0
C NZ=NZ+1
C WRITE (6,10) I,X(I),I
C CONTINUE
C K2=K+MO-2+NZ
30 IF (N.GT.K2) RETURN
C WRITE (6,20)
C STOP
C END
CHECK201
CHECK202
CHECK203
CHECK204
CHECK205
CHECK206
CHECK207
CHECK208
CHECK209
CHECK210
CHECK211
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CHECK214
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CHECK223
CHECK224
CHECK225
CHECK226
CHECK227
CHECK228
CHECK229
CHECK230
CHECK231
CHECK232
CHECK233
CHECK234
CHECK235

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SUBROUTINE CHSCDF (X,NU,CDF)

PURPOSE--THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
FUNCTION VALUE FOR THE CHI-SQUARED DISTRIBUTION
WITH INTEGER DEGREES OF FREEDOM PARAMETER = NU.
THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
THE PROBABILITY DENSITY FUNCTION IS GIVEN
IN THE REFERENCES BELOW.

INPUT ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
WHICH THE CUMULATIVE DISTRIBUTION
FUNCTION IS TO BE EVALUATED.

--NU = THE INTEGER NUMBER OF DEGREES
OF FREEDOM.

OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
DISTRIBUTION FUNCTION VALUE.

OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
FUNCTION VALUE CDF FOR THE CHI-SQUARED DISTRIBUTION
WITH DEGREES OF FREEDOM PARAMETER = NU.

PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
RESTRICTIONS--X SHOULD BE NON-NEGATIVE.

--NU SHOULD BE A POSITIVE INTEGER VARIABLE.

OTHER DATAPAC SUBROUTINES NEEDED--NORCDF.

FORTAN LIBRARY SUBROUTINES NEEDED--DSQRT, DEXP.

MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.

LANGUAGE--ANSI FORTRAN.

REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS

SERIES 55, 1964, PAGE 941, FORMULAE 26.4.4 AND 26.4.5.

--JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE

DISTRIBUTIONS--1, 1970, PAGE 176,

FORMULA 28, AND PAGE 180, FORMULA 33.1.

--OWEN, HANDBOOK OF STATISTICAL TABLES,

1962, PAGES 50-55.

--PEARSON AND HARTLEY, BIOMETRIKA TABLES

FOR STATISTICIANS, VOLUME 1, 1954,

PAGES 122-131.

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WASHINGTON, D. C. 20234

PHONE: 301-921-2315

ORIGINAL VERSION--JUNE 1972.

UPDATED --MAY 1974.

UPDATED --SEPTEMBER 1975.

UPDATED --NOVEMBER 1975.

UPDATED --OCTOBER 1976.

DOUBLE PRECISION DX,PI,CHI,SUM,TERM,AI,DCDFN

DOUBLE PRECISION DNU

DOUBLE PRECISION DSQRT,DEXP

DOUBLE PRECISION DLOG

DOUBLE PRECISION DFACT,DPOWER

DOUBLE PRECISION DW

DOUBLE PRECISION D1,D2,D3

CHSCD001
CHSCD002
CHSCD003
CHSCD004
CHSCD005
CHSCD006
CHSCD007
CHSCD008
CHSCD009
CHSCD010
CHSCD011
CHSCD012
CHSCD013
CHSCD014
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CHSCD055
CHSCD056
CHSCD057

DOUBLE PRECISION TERM0, TERM1, TERM2, TERM3, TERM4
 DOUBLE PRECISION B11
 DOUBLE PRECISION B21
 DOUBLE PRECISION B31, B32
 DOUBLE PRECISION B41, B42, B43
 DATA NUCUT /1000/
 DATA PI /3.14159265358979D0/
 DATA DPOWER /0.3333333333333D0/
 DATA B11 /0.3333333333333D0/
 DATA B21 /-0.027777777777778D0/
 DATA B31 /-0.00061728395061D0/
 DATA B32 /-13.0D0/
 DATA B41 /0.00018004115226D0/
 DATA B42 /6.0D0/
 DATA B43 /17.0D0/
 IPR=6
 CHECK THE INPUT ARGUMENTS FOR ERRORS
 IF (NU.LE.0) GO TO 10
 IF (X.LT.0.0) GO TO 20
 GO TO 30
 WRITE (IPR,50)
 WRITE (IPR,70) NU
 CDF=0.0
 RETURN
 WRITE (IPR,40)
 WRITE (IPR,60) X
 CDF=0.0
 RETURN
 CONTINUE
 FORMAT (1H,96H***** NON-FATAL DIAGNOSTIC--THE FIRST INPUT ARGUMENT CHSCD090
 2NT TO THE CHSCDF SUBROUTINE IS NEGATIVE *****)
 50 FORMAT (1H,91H***** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THECHSCD092
 2 CHSCDF SUBROUTINE IS NON-POSITIVE *****)
 60 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,E15.8,6H *****)
 70 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,18,6H *****)
 C-----START POINT-----
 C
 DX=X
 ANU=NU
 DNU=NU
 C
 IF X IS NON-POSITIVE, SET CDF = 0.0 AND RETURN.
 IF NU IS SMALLER THAN 10 AND X IS MORE THAN 200
 STANDARD DEVIATIONS BELOW THE MEAN,
 SET CDF = 0.0 AND RETURN.
 IF NU IS 10 OR LARGER AND X IS MORE THAN 100
 STANDARD DEVIATIONS BELOW THE MEAN,
 SET CDF = 0.0 AND RETURN.
 IF NU IS SMALLER THAN 10 AND X IS MORE THAN 200
 STANDARD DEVIATIONS ABOVE THE MEAN,
 SET CDF = 1.0 AND RETURN.
 IF NU IS 10 OR LARGER AND X IS MORE THAN 100
 STANDARD DEVIATIONS ABOVE THE MEAN,
 SET CDF = 1.0 AND RETURN.

CHSCD058
 CHSCD059
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116 C
117 IF (X.LE.0.0) GO TO 80
118 AMEAN=ANU
119 SD=SQRT(2.0*ANU)
120 Z=(X-AMEAN)/SD
121 IF (NU.LT.10.AND.Z.LT.-200.0) GO TO 80
122 IF (NU.GE.10.AND.Z.LT.-100.0) GO TO 80
123 IF (NU.LT.10.AND.Z.GT.200.0) GO TO 90
124 IF (NU.GE.10.AND.Z.GT.100.0) GO TO 90
125 GO TO 100
126 CDF=0.0
127 RETURN
128 CDF=1.0
129 RETURN
130 CONTINUE
131 C
132 DISTINGUISH BETWEEN 3 SEPARATE REGIONS
133 OF THE (X,NU) SPACE.
134 BRANCH TO THE PROPER COMPUTATIONAL METHOD
135 DEPENDING ON THE REGION.
136 NUCUT HAS THE VALUE 1000.
137 C
138 IF (NU.LT.NUCUT) GO TO 120
139 IF (NU.GE.NUCUT.AND.X.LE.ANU) GO TO 180
140 IF (NU.GE.NUCUT.AND.X.GT.ANU) GO TO 190
141 IBRAN=1
142 WRITE (IPR,110) IBRAN
143 FORMAT (1H,42H****INTERNAL ERROR IN CHSCDF SUBROUTINE--,
144 2 46HIMPOSSIBLE BRANCH CONDITION AT BRANCH POINT = ,18)
145 RETURN
146 C
147 TREAT THE SMALL AND MODERATE DEGREES OF FREEDOM CASE
148 (THAT IS, WHEN NU IS SMALLER THAN 1000).
149 METHOD UTILIZED--EXACT FINITE SUM
150 (SEE AMS 55, PAGE 941, FORMULAE 26.4.4 AND 26.4.5).
151 C
152 CONTINUE
153 CHI=DSQRT(DX)
154 IEVODD=NU-2*(NU/2)
155 IF (IEVODD.EQ.0) GO TO 130
156 C
157 SUM=0.0D0
158 TERM=1.0/CHI
159 IMIN=1
160 IMAX=NU-1
161 GO TO 140
162 C
163 SUM=1.0D0
164 TERM=1.0D0
165 IMIN=2
166 IMAX=NU-2
167 C
168 IF (IMIN.GT.IMAX) GO TO 160
169 DO 150 I=IMIN,IMAX,2
170 AI=I
171 TERM=TERM*(DX/AI)
172 SUM=SUM+TERM
173 CONTINUE

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174 CHSCD174
175 CHSCD175
176 CHSCD176
177 CHSCD177
178 CHSCD178
179 CHSCD179
180 CHSCD180
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218 CHSCD218
219 CHSCD219
220 CHSCD220
221 CHSCD221

160 CONTINUE
C
SUM=SUM*DEXP(-DX/2.0D0)
IF (IEVODD.EQ.0) GO TO 170
SUM=(DSQRT(2.0D0/PI))*SUM
SPCHI=CHI
CALL NORCDF (SPCHI, CDFN)
DCDFN=CDFN
SUM=SUM+2.0D0*(1.0D0-DCDFN)
CDF=1.0D0-SUM
RETURN
170
C
TREAT THE CASE WHEN NU IS LARGE
(THAT IS, WHEN NU IS EQUAL TO OR GREATER THAN 1000)
AND X IS LESS THAN OR EQUAL TO NU.
METHOD UTILIZED--WILSON-HILFERTY APPROXIMATION
(SEE JOHNSON AND KOTZ, VOLUME 1, PAGE 176, FORMULA 28).
180 CONTINUE
DFACT=4.5D0*DNU
U=((DX/DNU)**DPOWER)-1.0D0+(1.0D0/DFACT))*DSQRT(DFACT)
CALL NORCDF (U, CDFN)
CDF=CDFN
RETURN
C
TREAT THE CASE WHEN NU IS LARGE
(THAT IS, WHEN NU IS EQUAL TO OR GREATER THAN 1000)
AND X IS LARGER THAN NU.
METHOD UTILIZED--HILL'S ASYMPTOTIC EXPANSION
(SEE JOHNSON AND KOTZ, VOLUME 1, PAGE 180, FORMULA 33.1).
190 CONTINUE
DW=DSQRT(DX-DNU-DNU*DLOG(DX/DNU))
DANU=DSQRT(2.0D0/DNU)
D1=DW
D2=DW**2
D3=DW**3
TERM0=DW
TERM1=B11*DANU
TERM2=B21*D1*(DANU**2)
TERM3=B31*(D2+B32)*(DANU**3)
TERM4=B41*(B42*D3+B43*D1)*(DANU**4)
U=TERM0+TERM1+TERM2+TERM3+TERM4
CALL NORCDF (U, CDFN)
CDF=CDFN
RETURN
C
END

```


SUBROUTINE CHSPPF (P,NU,PPF)

PURPOSE--THIS SUBROUTINE COMPUTES THE PERCENT POINT FUNCTION VALUE FOR THE CHI-SQUARED DISTRIBUTION WITH INTEGER DEGREES OF FREEDOM PARAMETER = NU. THE CHI-SQUARED DISTRIBUTION USED HEREIN IS DEFINED FOR ALL NON-NEGATIVE X, AND ITS PROBABILITY DENSITY FUNCTION IS GIVEN IN REFERENCES 2, 3, AND 4 BELOW.

NOTE THAT THE PERCENT POINT FUNCTION OF A DISTRIBUTION IS IDENTICALLY THE SAME AS THE INVERSE CUMULATIVE DISTRIBUTION FUNCTION OF THE DISTRIBUTION.

INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE (BETWEEN 0.0 (INCLUSIVELY) AND 1.0 (EXCLUSIVELY)) AT WHICH THE PERCENT POINT FUNCTION IS TO BE EVALUATED.

--NU = THE INTEGER NUMBER OF DEGREES OF FREEDOM.

NU SHOULD BE POSITIVE.

OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT POINT FUNCTION VALUE.

OUTPUT--THE SINGLE PRECISION PERCENT POINT FUNCTION VALUE PPF FOR THE CHI-SQUARED DISTRIBUTION WITH DEGREES OF FREEDOM PARAMETER = NU.

PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.

RESTRICTIONS--NU SHOULD BE A POSITIVE INTEGER VARIABLE.

--P SHOULD BE BETWEEN 0.0 (INCLUSIVELY) AND 1.0 (EXCLUSIVELY).

OTHER DATAPAC SUBROUTINES NEEDED--NONE.

FORTAN LIBRARY SUBROUTINES NEEDED--DEXP, DLOG.

MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.

LANGUAGE--ANSI FORTRAN.

ACCURACY--(ON THE UNIVAC 1108, EXEC 8 SYSTEM AT NBS) COMPARED TO THE KNOWN NU = 2 (EXPONENTIAL) RESULTS, AGREEMENT WAS HAD OUT TO 6 SIGNIFICANT DIGITS FOR ALL TESTED P IN THE RANGE P = .001 TO P = .999. FOR P = .95 AND SMALLER, THE AGREEMENT WAS EVEN BETTER--7 SIGNIFICANT DIGITS.

(NOTE THAT THE TABULATED VALUES GIVEN IN THE WILK, GNANADESIKAN, AND HUYETT REFERENCE BELOW, PAGE 20, ARE IN ERROR FOR AT LEAST THE GAMMA = 1 CASE--THE WORST DETECTED ERROR WAS AGREEMENT TO ONLY 3 SIGNIFICANT DIGITS (IN THEIR 8 SIGNIFICANT DIGIT TABLE) FOR P = .999.)

REFERENCES--WILK, GNANADESIKAN, AND HUYETT, 'PROBABILITY PLOTS FOR THE GAMMA DISTRIBUTION', TECHNOMETRICS, 1962, PAGES 1-15, ESPECIALLY PAGES 3-5.

--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS SERIES 55, 1964, PAGE 257, FORMULA 6.1.41, AND PAGES 940-943.

--JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE DISTRIBUTIONS--1, 1970, PAGES 166-206.

--HASTINGS AND PEACOCK, STATISTICAL DISTRIBUTIONS--A HANDBOOK FOR STUDENTS AND PRACTITIONERS, 1975,

CHSPPF001
CHSPPF002
CHSPPF003
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CHSP0059 CHSP0060 CHSP0061 CHSP0062 CHSP0064 CHSP0065 CHSP0066 CHSP0067 CHSP0068 CHSP0069 CHSP0070 CHSP0071 CHSP0072 CHSP0073 CHSP0074 CHSP0075 CHSP0076 CHSP0077 CHSP0078 CHSP0079 CHSP0080 CHSP0081 CHSP0082 CHSP0083 CHSP0084 CHSP0085 CHSP0086 CHSP0087 CHSP0088 CHSP0089 CHSP0090 CHSP0091 CHSP0092 CHSP0093 CHSP0094 CHSP0095 CHSP0096 CHSP0097 CHSP0098 CHSP0099 CHSP0100 CHSP0101 CHSP0102 CHSP0103 CHSP0104 CHSP0105 CHSP0106 CHSP0107 CHSP0108 CHSP0109 CHSP0110 CHSP0111 CHSP0112 CHSP0113 CHSP0114 CHSP0115

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CHSPP 113
CHSPP 114
CHSPP 115

CHSPP:1.14
CHSPP:1.15

41


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116 DP=P
117 DNU=NU
118 DCAMMA=DNU/2.0D0
119 MAXIT=10000
120
121 C COMPUTE THE GAMMA FUNCTION USING THE ALGORITHM IN THE
122 C NBS APPLIED MATHEMATICS SERIES REFERENCE.
123 C THIS GAMMA FUNCTION NEED BE CALCULATED ONLY ONCE.
124 C IT IS USED IN THE CALCULATION OF THE CDF BASED ON
125 C THE TENTATIVE VALUE OF THE PPF IN THE ITERATION.
126 C
127 Z=DCAMMA
128 DEN=1.0D0
129 IF (Z.GE.10.0D0) GO TO 90
130 DER=DEN*Z
131 Z=Z+1.0D0
132 GO TO 80
133 Z2=Z*Z
134 Z3=Z*Z2
135 Z4=Z2*Z2
136 Z5=Z2*Z3
137 A=(Z-0.5D0)*DLOG(Z)-Z+C
138 B=D(1)/Z+D(2)/Z3+D(3)/Z5+D(4)/(Z2*Z3)+D(5)/(Z4*Z3)+D(6)/(Z4*Z3*Z5)+
139 2D(7)/(Z3*Z5*Z3)+D(8)/(Z5*Z3*Z5)+D(9)/(Z2*Z3*Z3*Z3)
140 C=DEXP(A+B)/DEN
141
142 C DETERMINE LOWER AND UPPER LIMITS ON THE DESIRED 100P
143 C PERCENT POINT.
144 C
145 ILOOP=1
146 XMIN=(DP*DCAMMA+C)**(1.0D0/DCAMMA)
147 XMIN=XMIN0
148 ICOUNT=1
149 AI=ICOUNT
150 XMAX=AI*XMIN0
151 DX=XMAX
152 GO TO 180
153 IF (PCALC.GE.DP) GO TO 120
154 XMIN=XMAX
155 ICOUNT=ICOUNT+1
156 IF (ICOUNT.LE.30000) GO TO 100
157 X MID=(XMIN+XMAX)/2.0D0
158
159 C NOW ITERATE BY BISECTION UNTIL THE DESIRED ACCURACY IS ACHIEVED.
160 C
161 ILOOP=2
162 XLOWER=XMIN
163 XUPPER=XMAX
164 ICOUNT=0
165 DX=X MID
166 GO TO 180
167 IF (PCALC.EQ.DP) GO TO 170
168 IF (PCALC.GT.DP) GO TO 150
169 XLOWER=X MID
170 X MID=(X MID+XUPPER)/2.0D0
171 GO TO 160
172 XUPPER=X MID
173 X MID=(X MID+XLOWER)/2.0D0

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174 CHSPP174
175 CHSPP175
176 CHSPP176
177 CHSPP177
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213 CHSPP213
214 CHSPP214
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218 CHSPP218
219 CHSPP219
220 CHSPP220

160 XDEL=XMID-XLOWER
    IF (XDEL.LT.0.0D0) XDEL=-XDEL
    ICOUNT=ICOUNT+1
    IF (XDEL.LT.0.000000001D0.OR.ICOUNT.GT.100) GO TO 170
    GO TO 130
170 PPF=2.0D0*XMID
    RETURN
C *****
C THIS SECTION BELOW IS LOGICALLY SEPARATE FROM THE ABOVE.
C THIS SECTION COMPUTES A CDF VALUE FOR ANY GIVEN TENTATIVE
C PERCENT POINT X VALUE AS DEFINED IN EITHER OF THE 2
C ITERATION LOOPS IN THE ABOVE CODE.
C *****
C COMPUTE T-SUB-Q AS DEFINED ON PAGE 4 OF THE WILK, GNANADESIKAN,
C AND HUYETT REFERENCE
C *****
180 SUM=1.0D0/DCAMMA
    TERM=1.0D0/DCAMMA
    CUT1=DX-DCAMMA
    CUT2=DX*10000000000.0D0
    DO 190 J=1,MAXIT
    AJ=J
    TERM=DX*TERM/(DCAMMA+AJ)
    SUM=SUM+TERM
    CUTOFF=CUT1+(CUT2*TERM/SUM
    IF (AJ.GT.CUTOFF) GO TO 200
190 CONTINUE
    WRITE (IPR,210) MAXIT
    WRITE (IPR,220) P
    WRITE (IPR,230) NU
    WRITE (IPR,240)
    PPF=0.0
    RETURN
C *****
200 T=SUM
    PCALC=(DX**DCAMMA)*(DEXP(-DX))*T/G
    IF (ILOOP.EQ.1) GO TO 110
    GO TO 140
C *****
210 FORMAT (1H,48H*****ERROR IN INTERNAL OPERATIONS IN THE CHSPPF,
2 45HSUBROUTINE--THE NUMBER OF ITERATIONS EXCEEDS,17)
220 FORMAT (1H,33H THE INPUT VALUE OF P IS,E15.8)
230 FORMAT (1H,33H THE INPUT VALUE OF NU IS,18)
240 FORMAT (1H,48H THE OUTPUT VALUE OF PPF HAS BEEN SET TO 0.0)
C *****
    END

```

CPR*NS(1).CIYFIN(6)

```

1 SUBROUTINE CIYFIN (XF,YF,YFSD,NF,RSD,AL,DL,C,NRSD,NB,YFL,YFU,IP) CIYFIN01
2 C----- CIYFIN02
3 C CIYFIN WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C. CIYFIN03
5 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION CIYFIN04
6 C FOR: COMPUTING CONFIDENCE INTERVALS FOR PREDICTED Y-VALUES ON A CIYFIN05
7 C CALIBRATION CURVE USING SCHEFFE'S TECHNIQUE CIYFIN06
8 C CIYFIN07
9 C CIYFIN08
10 C REFERENCE: SCHEFFE, HENRY, 'A STATISTICAL THEORY OF CALIBRATION' CIYFIN09
11 C THE ANNALS OF STATISTICS, VOLUME 1, NUMBER 1 CIYFIN10
12 C JANUARY 1973, PP. 1-37 CIYFIN11
13 C CIYFIN12
14 C SUBPROGRAMS CALLED: CHSPFF, FPPF, NORPPF CIYFIN13
15 C CURRENT VERSION COMPLETED MARCH 17, 1980 CIYFIN14
16 C----- CIYFIN15
17 C DIMENSION XF(NF), YF(NF), YFSD(NF), YFL(NF), YFU(NF) CIYFIN16
18 C WRITE FORMATS CIYFIN17
19 C FORMAT (15X,2HZ(,F7.5,3H) =,F11.5) CIYFIN18
20 C FORMAT (6X,6HCHISQ(,F7.5,1H,,14,3H) =,F11.5) CIYFIN19
21 C FORMAT (5X,2HF(,F7.5,1H,,14,1H,,14,3H) =,F11.5) CIYFIN20
22 C FORMAT (/1X,75(1H-)/1X,26H* CONFIDENCE INTERVALS FOR,15,1X, CIYFIN21
23 C 2 43HEVENLY SPACED POINTS WITHIN THE KNOT SPAN */1X,75(1H-)/5X, CIYFIN22
24 C 3 7HALPHA =,F8.5,5X,7HDELTA =,F8.5,5X,3HC =,F5.2/) CIYFIN23
25 C FORMAT (1X,14,5G13.6) CIYFIN24
26 C FORMAT (/20X,9HPREDICTED 5X,7HSTD DEV,6X,19HCONFIDENCE INTERVAL/ CIYFIN25
27 C 2 4X,1HI,5X,4HX(1),9X,4HY(1),6X,9HPRED Y(1),6X,5HLOWER,8X,5HUPPER/) CIYFIN26
28 C WRITE (6,40) NF,AL,DL,C CIYFIN27
29 C COMPUTE Z(1-AL/2) CRITICAL POINT FOR N(0,1) P.D.F. CIYFIN28
30 C P=1.0-AL/2.0 CIYFIN29
31 C CALL NORPPF (P,ZAL) CIYFIN30
32 C WRITE (6,10) P,ZAL CIYFIN31
33 C----- ARTIFICIALLY SET NEXT TWO CRITICAL POINTS IF DELTA=1 CIYFIN32
34 C CDL=NRSD CIYFIN33
35 C FDL=0 CIYFIN34
36 C IF (DL.EQ.1.0) GO TO 70 CIYFIN35
37 C COMPUTE CHISQ(DL) CRITICAL POINT FOR CHI-SQUARED(NRSD) P.D.F. CIYFIN36
38 C CALL CHSPFF (DL,NRSD,CDL) CIYFIN37
39 C WRITE (6,20) DL,NRSD,CDL CIYFIN38
40 C COMPUTE F(1-DL) CRITICAL POINT FOR F(NB,NRSD) P.D.F. CIYFIN39
41 C CALL FPPF (P,NB,NRSD,FDL) CIYFIN40
42 C WRITE (6,30) P,NB,NRSD,FDL CIYFIN41
43 C----- COMPUTE CONFIDENCE INTERVAL FOR EACH Y VALUE CIYFIN42
44 C C1=ZAL*SQRT(FLOAT(NRSD)/CDL) CIYFIN43
45 C C2=SQRT(FLOAT(NB)*FDL) CIYFIN44
46 C C3=C*NRSD CIYFIN45
47 C DO 80 I=1,NF CIYFIN46
48 C WIDTH=C3*(C1+C2*YFSD(I)) CIYFIN47
49 C YFL(I)=YF(I)-WIDTH CIYFIN48
50 C YFU(I)=YF(I)+WIDTH CIYFIN49
51 C CONTINUE CIYFIN50
52 C----- CHECK WHETHER TO PRINT OUT EACH Y VALUE AND ITS STANDARD DEVIATION CIYFIN51
53 C IF (IP.LT.2) GO TO 100 CIYFIN52
54 C----- PRINT OUT EACH Y VALUE AND ITS STANDARD DEVIATION CIYFIN53
55 C WRITE (6,60) CIYFIN54
56 C DO 90 I=1,NF CIYFIN55
57 C WRITE (6,50) I,XF(I),YF(I),YFSD(I),YFL(I),YFU(I) CIYFIN56

```

CIYFIN58
CIYFIN59
CIYFIN60
CIYFIN61
CIYFIN62
CIYFIN63
CIYFIN64

90 CONTINUE
RETURN
100 WRITE (6,110)
110 FORMAT (/1X,43H***** PRINTOUT OF Y CONFIDENCE INTERVALS ,
2 18HSUPPRESSED *****)
RETURN
END

58
59
60
61
62
63
64

CPR*NS(1).COVAR(2)

SUBROUTINE COVAR (NMX,N,KMX,K,Q,CI)

INTEGER NMX,N,KMX,K

REAL Q(KMX,N),CI(NMX,N)

THIS FORTRAN SUBROUTINE COMPUTES AND RETURNS THE N X N UNSCALED
COVARIANCE MATRIX CI OBTAINED BY INVERTING THE GRAMIAN MATRIX C. THE
CHOLESKY FACTOR L OF C IS ASSUMED TO BE STORED IN Q ON INPUT.
SUBROUTINE BCHSLV IS USED TO SOLVE FOR EACH COLUMN OF THE INVERSE.

ON INPUT.

NMX IS THE ROW DIMENSION OF CI.

N IS THE DIMENSION OF THE SPACE OF SPLINES OF ORDER
K.

KMX IS THE ROW DIMENSION OF Q.

K IS THE ORDER OF THE SPLINES = DEGREE + 1

Q(*,*) HAS ROW DIMENSION KMX AND COLUMN DIMENSION AT LEAST
N. THE CHOLESKY FACTOR L OF C IS STORED IN THE
FIRST K ROWS OF THE MATRIX.

ON OUTPUT.

CI(*,*) HAS ROW DIMENSION NMX AND COLUMN DIMENSION AT LEAST
N. IT CONTAINS THE UNSCALED COVARIANCE MATRIX IN
STANDARD ROW, COLUMN FORM.

AND THE REST OF THE VARIABLES ARE UNCHANGED.

ADDITIONAL ROUTINES REQUIRED.

BCHSLV

BY.

MARTIN CORDES
CENTER FOR APPLIED MATHEMATICS, NBS
VERSION 1 - OCT 1979

INTEGER I,J

DO 20 J=1,N

DO 10 I=1,N

CI(I,J)=0.0

CONTINUE

CI(J,J)=1.0

CALL BCHSLV (Q,KMX,K,N,CI(1,J))

CONTINUE

RETURN

END

COVAR001
COVAR002
COVAR003
COVAR004
COVAR005
COVAR006
COVAR007
COVAR008
COVAR009
COVAR010
COVAR011
COVAR012
COVAR013
COVAR014
COVAR015
COVAR016
COVAR017
COVAR018
COVAR019
COVAR020
COVAR021
COVAR022
COVAR023
COVAR024
COVAR025
COVAR026
COVAR027
COVAR028
COVAR029
COVAR030
COVAR031
COVAR032
COVAR033
COVAR034
COVAR035
COVAR036
COVAR037
COVAR038
COVAR039
COVAR040
COVAR041
COVAR042
COVAR043
COVAR044
COVAR045
COVAR046
COVAR047
COVAR048
COVAR049
COVAR050
COVAR051
COVAR052
COVAR053
COVAR054
COVAR055
COVAR056
COVAR057

SUBROUTINE FCDF (X,NU1,NU2,CDF)

PURPOSE--THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
FUNCTION VALUE FOR THE F DISTRIBUTION
WITH INTEGER DEGREES OF FREEDOM
PARAMETERS = NU1 AND NU2.

THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
THE PROBABILITY DENSITY FUNCTION IS GIVEN
IN THE REFERENCES BELOW.

INPUT ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
WHICH THE CUMULATIVE DISTRIBUTION
FUNCTION IS TO BE EVALUATED.

--NU1 = THE INTEGER DEGREES OF FREEDOM
FOR THE NUMERATOR OF THE F RATIO.

--NU2 = THE INTEGER DEGREES OF FREEDOM
FOR THE DENOMINATOR OF THE F RATIO.
NU2 SHOULD BE POSITIVE.

OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
DISTRIBUTION FUNCTION VALUE.

OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
FUNCTION VALUE CDF FOR THE F DISTRIBUTION
WITH DEGREES OF FREEDOM
PARAMETERS = NU1 AND NU2.

PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
RESTRICTIONS--X SHOULD BE NON-NEGATIVE.

--NU1 SHOULD BE A POSITIVE INTEGER VARIABLE.
--NU2 SHOULD BE A POSITIVE INTEGER VARIABLE.

OTHER DATAPAC SUBROUTINES NEEDED--NORCDF, CHSCDF.
FORTRAN LIBRARY SUBROUTINES NEEDED--DSQRT, DATAN.
MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.
LANGUAGE--ANSI FORTRAN.

REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS

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UPDATED --NOVEMBER 1975.

UPDATED --OCTOBER 1976.

FCDF0001
FCDF0002
FCDF0003
FCDF0004
FCDF0005
FCDF0006
FCDF0007
FCDF0008
FCDF0009
FCDF0010
FCDF0011
FCDF0012
FCDF0013
FCDF0014
FCDF0015
FCDF0016
FCDF0017
FCDF0018
FCDF0019
FCDF0020
FCDF0021
FCDF0022
FCDF0023
FCDF0024
FCDF0025
FCDF0026
FCDF0027
FCDF0028
FCDF0029
FCDF0030
FCDF0031
FCDF0032
FCDF0033
FCDF0034
FCDF0035
FCDF0036
FCDF0037
FCDF0038
FCDF0039
FCDF0040
FCDF0041
FCDF0042
FCDF0043
FCDF0044
FCDF0045
FCDF0046
FCDF0047
FCDF0048
FCDF0049
FCDF0050
FCDF0051
FCDF0052
FCDF0053
FCDF0054
FCDF0055
FCDF0056
FCDF0057

```

58 C
59
60 DOUBLE PRECISION DX,PI,ANU1,ANU2,Z,SUM,TERM,AI,COEF1,COEF2,ARG
61 DOUBLE PRECISION COEF
62 DOUBLE PRECISION THETA,SINTH,COSTH,A,B
63 DOUBLE PRECISION DSQRT,DATAN
64 DOUBLE PRECISION DFACT1,DFACT2,DNUM,DDEN
65 DOUBLE PRECISION DPOW1,DPOW2
66 DOUBLE PRECISION DNU1,DNU2
67 DOUBLE PRECISION TERM1,TERM2,TERM3
68 DATA PI /3.14159265358979D0/
69 DATA DPOW1,DPOW2 /0.33333333333333D0,0.666666666666667D0/
70 DATA NUCUT1,NUCUT2 /100,1000/
71 C
72 IPR=6
73 C
74 CHECK THE INPUT ARGUMENTS FOR ERRORS
75
76 IF (NU1.LE.0) GO TO 10
77 IF (NU2.LE.0) GO TO 20
78 IF (X.LT.0.0) GO TO 30
79 GO TO 40
80 WRITE (IPR,60)
81 WRITE (IPR,90) NU1
82 CDF=0.0
83 RETURN
84 WRITE (IPR,70)
85 WRITE (IPR,90) NU2
86 CDF=0.0
87 RETURN
88 WRITE (IPR,50)
89 WRITE (IPR,80) X
90 CDF=0.0
91 RETURN
92 CONTINUE
93 FORMAT (1H,96H***** NON-FATAL DIAGNOSTIC--THE FIRST INPUT ARGUMENT
94 2NT TO THE FCDF SUBROUTINE IS NEGATIVE *****)
95 FORMAT (1H,91H***** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THEFCDF0094
96 2 FCDF SUBROUTINE IS NON-POSITIVE *****)
97 FORMAT (1H,91H***** FATAL ERROR--THE THIRD INPUT ARGUMENT TO THEFCDF0096
98 2 FCDF SUBROUTINE IS NON-POSITIVE *****)
99 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,E15.8,6H *****)
100 FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,I8,6H *****)
101 C
102 C-----START POINT-----
103 C
104 DX=X
105 M=NU1
106 N=NU2
107 ANU1=NU1
108 ANU2=NU2
109 DNU1=NU1
110 DNU2=NU2
111 C
112 IF X IS NON-POSITIVE, SET CDF = 0.0 AND RETURN.
113 IF NU2 IS 5 THROUGH 9 AND X IS MORE THAN 3000
114 STANDARD DEVIATIONS BELOW THE MEAN,
115 SET CDF = 0.0 AND RETURN.
116 IF NU2 IS 10 OR LARGER AND X IS MORE THAN 150

```



```

116 C STANDARD DEVIATIONS BELOW THE MEAN,
117 C SET CDF = 0.0 AND RETURN.
118 C IF NU2 IS 5 THROUGH 9 AND X IS MORE THAN 3000
119 C STANDARD DEVIATIONS ABOVE THE MEAN,
120 C SET CDF = 1.0 AND RETURN.
121 C IF NU2 IS 10 OR LARGER AND X IS MORE THAN 150
122 C STANDARD DEVIATIONS ABOVE THE MEAN,
123 C SET CDF = 1.0 AND RETURN.
124 C
125 C IF (X.LE.0.0) GO TO 100
126 C IF (NU2.LE.4) GO TO 120
127 C T1=2.0/ANU1
128 C T2=ANU2/(ANU2-2.0)
129 C T3=(ANU1+ANU2-2.0)/(ANU2-4.0)
130 C AMEAN=T2
131 C SD=SQRT(T1*T2*T2*T3)
132 C ZRATIO=(X-AMEAN)/SD
133 C IF (NU2.LT.10.AND.ZRATIO.LT.-3000.0) GO TO 100
134 C IF (NU2.GE.10.AND.ZRATIO.LT.-150.0) GO TO 100
135 C IF (NU2.LT.10.AND.ZRATIO.GT.3000.0) GO TO 110
136 C IF (NU2.GE.10.AND.ZRATIO.GT.150.0) GO TO 110
137 C GO TO 120
138 C CDF=0.0
139 C RETURN
140 C CDF=1.0
141 C RETURN
142 C CONTINUE
143 C
144 C DISTINGUISH BETWEEN 6 SEPARATE REGIONS
145 C OF THE (NU1,NU2) SPACE.
146 C BRANCH TO THE PROPER COMPUTATIONAL METHOD
147 C DEPENDING ON THE REGION.
148 C NUCUT1 HAS THE VALUE 100.
149 C NUCUT2 HAS THE VALUE 1000.
150 C
151 C IF (NU1.LT.NUCUT2.AND.NU2.LT.NUCUT2) GO TO 140
152 C IF (NU1.GE.NUCUT2.AND.NU2.GE.NUCUT2) GO TO 310
153 C IF (NU1.LT.NUCUT1.AND.NU2.GE.NUCUT2) GO TO 320
154 C IF (NU1.GE.NUCUT1.AND.NU2.GE.NUCUT2) GO TO 310
155 C IF (NU1.GE.NUCUT2.AND.NU2.LT.NUCUT1) GO TO 330
156 C IF (NU1.GE.NUCUT2.AND.NU2.GE.NUCUT1) GO TO 310
157 C IBRAN=5
158 C WRITE (IPR,130) IBRAN
159 C FORMAT (1H,42H****INTERNAL ERROR IN FCDF SUBROUTINE--,
160 C 2 46HIMPOSSIBLE BRANCH CONDITION AT BRANCH POINT = ,18)
161 C RETURN
162 C
163 C TREAT THE CASE WHEN NU1 AND NU2
164 C ARE BOTH SMALL OR MODERATE
165 C (THAT IS, BOTH ARE SMALLER THAN 1000).
166 C METHOD UTILIZED--EXACT FINITE SUM
167 C (SEE AMS 55, PAGE 946, FORMULAE 26.6.4, 26.6.5,
168 C AND 26.6.8).
169 C
170 C CONTINUE
171 C Z=ANU2/(ANU2+ANU1*DX)
172 C IFLAG1=NU1-2*(NU1/2)
173 C IFLAG2=NU2-2*(NU2/2)

```

```

FCDF0116
FCDF0117
FCDF0118
FCDF0119
FCDF0120
FCDF0121
FCDF0122
FCDF0123
FCDF0124
FCDF0125
FCDF0126
FCDF0127
FCDF0128
FCDF0129
FCDF0130
FCDF0131
FCDF0132
FCDF0133
FCDF0134
FCDF0135
FCDF0136
FCDF0137
FCDF0138
FCDF0139
FCDF0140
FCDF0141
FCDF0142
FCDF0143
FCDF0144
FCDF0145
FCDF0146
FCDF0147
FCDF0148
FCDF0149
FCDF0150
FCDF0151
FCDF0152
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FCDF0161
FCDF0162
FCDF0163
FCDF0164
FCDF0165
FCDF0166
FCDF0167
FCDF0168
FCDF0169
FCDF0170
FCDF0171
FCDF0172
FCDF0173

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174 IF (IFLAG1.EQ.0) GO TO 150
175 IF (IFLAG2.EQ.0) GO TO 180
176 GO TO 210
177
178 DO THE NU1 EVEN AND NU2 EVEN OR ODD CASE
179 C
180 SUM=0.0D0
181 TERM=1.0D0
182 IMAX=(N-2)/2
183 IF (IMAX.LE.0) GO TO 170
184 DO 160 I=1,IMAX
185 AI=I
186 COEF1=2.0D0*(AI-1.0D0)
187 COEF2=2.0D0*AI
188 TERM=TERM*((ANU2+COEF1)/COEF2)*(1.0D0-Z)
189 SUM=SUM+TERM
190 CONTINUE
191
192 SUM=SUM+1.0D0
193 SUM=(Z**((ANU2/2.0D0))*SUM
194 CDF=1.0D0-SUM
195 RETURN
196
197 DO THE NU1 ODD AND NU2 EVEN CASE
198 C
199 SUM=0.0D0
200 TERM=1.0D0
201 IMAX=(N-2)/2
202 IF (IMAX.LE.0) GO TO 200
203 DO 190 I=1,IMAX
204 AI=I
205 COEF1=2.0D0*(AI-1.0D0)
206 COEF2=2.0D0*AI
207 TERM=TERM*((ANU1+COEF1)/COEF2)*Z
208 SUM=SUM+TERM
209 CONTINUE
210
211 SUM=SUM+1.0D0
212 CDF=((1.0D0-Z)**(ANU1/2.0D0))*SUM
213 RETURN
214
215 DO THE NU1 ODD AND NU2 ODD CASE
216 C
217 SUM=0.0D0
218 TERM=1.0D0
219 ARG=DSQRT((ANU1/ANU2)*DX)
220 THETA=DATAN(ARG)
221 SINTH=ARG/DSQRT(1.0D0+ARG*ARG)
222 COSTH=1.0D0/DSQRT(1.0D0+ARG*ARG)
223 IF (N.EQ.1) GO TO 240
224 IF (N.EQ.3) GO TO 230
225 IMAX=N-2
226 DO 220 I=3,IMAX,2
227 AI=I
228 COEF1=AI-1.0D0
229 COEF2=AI
230 TERM=TERM*(COEF1/COEF2)*(COSTH*COSTH)
231 SUM=SUM+TERM

```

```

FCDF0174
FCDF0175
FCDF0176
FCDF0177
FCDF0178
FCDF0179
FCDF0180
FCDF0181
FCDF0182
FCDF0183
FCDF0184
FCDF0185
FCDF0186
FCDF0187
FCDF0188
FCDF0189
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FCDF0191
FCDF0192
FCDF0193
FCDF0194
FCDF0195
FCDF0196
FCDF0197
FCDF0198
FCDF0199
FCDF0200
FCDF0201
FCDF0202
FCDF0203
FCDF0204
FCDF0205
FCDF0206
FCDF0207
FCDF0208
FCDF0209
FCDF0210
FCDF0211
FCDF0212
FCDF0213
FCDF0214
FCDF0215
FCDF0216
FCDF0217
FCDF0218
FCDF0219
FCDF0220
FCDF0221
FCDF0222
FCDF0223
FCDF0224
FCDF0225
FCDF0226
FCDF0227
FCDF0228
FCDF0229
FCDF0230
FCDF0231

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232	FCDF0232
233	FCDF0233
234	FCDF0234
235	FCDF0235
236	FCDF0236
237	FCDF0237
238	FCDF0238
239	FCDF0239
240	FCDF0240
241	FCDF0241
242	FCDF0242
243	FCDF0243
244	FCDF0244
245	FCDF0245
246	FCDF0246
247	FCDF0247
248	FCDF0248
249	FCDF0249
250	FCDF0250
251	FCDF0251
252	FCDF0252
253	FCDF0253
254	FCDF0254
255	FCDF0255
256	FCDF0256
257	FCDF0257
258	FCDF0258
259	FCDF0259
260	FCDF0260
261	FCDF0261
262	FCDF0262
263	FCDF0263
264	FCDF0264
265	FCDF0265
266	FCDF0266
267	FCDF0267
268	FCDF0268
269	FCDF0269
270	FCDF0270
271	FCDF0271
272	FCDF0272
273	FCDF0273
274	FCDF0274
275	FCDF0275
276	FCDF0276
277	FCDF0277
278	FCDF0278
279	FCDF0279
280	FCDF0280
281	FCDF0281
282	FCDF0282
283	FCDF0283
284	FCDF0284
285	FCDF0285
286	FCDF0286
287	FCDF0287
288	FCDF0288
289	FCDF0289


```

290 DNUM=((1.0D0-DFACT2)*(DX**DPOW1))-((1.0D0-DFACT1)
291 DDEN=DSQRT((DFACT2*(DX**DPOW2))+DFACT1)
292 U=DNUM/DDEN
293 CALL NORCDF (U,GCDF)
294 CDF=GCDF
295 RETURN
296
297 C
298 C
299 C
300 C
301 C
302 C
303 C
304 C
305 C
306 C
307 C
308 C
309 C
310 C
311 C
312 C
313 C
314 C
315 C
316 C
317 C
318 C
319 C
320 C
321 C
322 C
323 C
324 C
325 C
326 C
327 C
328 C
329 C

DNUM=((1.0D0-DFACT2)*(DX**DPOW1))-((1.0D0-DFACT1)
DDEN=DSQRT((DFACT2*(DX**DPOW2))+DFACT1)
U=DNUM/DDEN
CALL NORCDF (U,GCDF)
CDF=GCDF
RETURN

TREAT THE CASE WHEN NU1 IS SMALL
AND NU2 IS LARGE
(THAT IS, WHEN NU1 IS SMALLER THAN 100.
AND NU2 IS EQUAL TO OR LARGER THAN 1000).
METHOD UTILIZED--SHEFFE-TUKEY APPROXIMATION
(SEE JOHNSON AND KOTZ, VOLUME 2, PAGE 84, THIRD FORMULA).

CONTINUE
TERM1=DNU1
TERM2=(DNU1/DNU2)*(0.5D0*DNU1-1.0D0)
TERM3=-((DNU1/DNU2)*0.5D0
U=((TERM1+TERM2)/((1.0D0/DX)-TERM3)
CALL CHSCDF (U,NU1,CCDF)
CDF=CCDF
RETURN

TREAT THE CASE WHEN NU2 IS SMALL
AND NU1 IS LARGE
(THAT IS, WHEN NU2 IS SMALLER THAN 100.
AND NU1 IS EQUAL TO OR LARGER THAN 1000).
METHOD UTILIZED--SHEFFE-TUKEY APPROXIMATION
(SEE JOHNSON AND KOTZ, VOLUME 2, PAGE 84, THIRD FORMULA).

CONTINUE
TERM1=DNU2
TERM2=(DNU2/DNU1)*(0.5D0*DNU2-1.0D0)
TERM3=-((DNU2/DNU1)*0.5D0
U=((TERM1+TERM2)/((DX-TERM3)
CALL CHSCDF (U,NU2,CCDF)
CDF=1.0-CCDF
RETURN

END

```

1 SUBROUTINE FPPF (P, NU1, NU2, PPF)
2
3 C
4 C
5 C
6 C
7 C
8 C
9 C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
18 C
19 C
20 C
21 C
22 C
23 C
24 C
25 C
26 C
27 C
28 C
29 C
30 C
31 C
32 C
33 C
34 C
35 C
36 C
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C

PURPOSE--THIS SUBROUTINE COMPUTES THE PERCENT POINT
FOR THE F DISTRIBUTION
WITH INTEGER DEGREES OF FREEDOM
PARAMETERS = NU1 AND NU2.
THIS DISTRIBUTION IS DEFINED FOR ALL NON-NEGATIVE X.
THE PROBABILITY DENSITY FUNCTION IS GIVEN
IN THE REFERENCES BELOW.

INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE
(BETWEEN 0.0 AND 1.0)
AT WHICH THE PERCENT POINT
FUNCTION IS TO BE EVALUATED.
--NU1 = THE INTEGER DEGREES OF FREEDOM
FOR THE NUMERATOR OF THE F RATIO.
NU1 SHOULD BE POSITIVE.
--NU2 = THE INTEGER DEGREES OF FREEDOM
FOR THE DENOMINATOR OF THE F RATIO.
NU2 SHOULD BE POSITIVE.

OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT POINT
FUNCTION VALUE.

OUTPUT--THE SINGLE PRECISION PERCENT POINT
FUNCTION VALUE PPF FOR THE F DISTRIBUTION
WITH DEGREES OF FREEDOM
PARAMETERS = NU1 AND NU2.

PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
RESTRICTIONS--P SHOULD BE BETWEEN
0.0 (INCLUSIVELY) AND 1.0 (EXCLUSIVELY).
--NU1 SHOULD BE A POSITIVE INTEGER VARIABLE.
--NU2 SHOULD BE A POSITIVE INTEGER VARIABLE.

OTHER DATAPAC SUBROUTINES NEEDED--FCDF, NORCDF, CHSCDF, NORPPF.
FORTRAN LIBRARY SUBROUTINES NEEDED--DSQRT, DATAN.
MODE OF INTERNAL OPERATIONS--DOUBLE PRECISION.

LANGUAGE--ANSI FORTRAN.

REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
SERIES 55, 1964, PAGES 946-947.
FORMULAE 26.6.4, 26.6.5, 26.6.8, AND 26.6.15.
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DISTRIBUTIONS--2, 1970, PAGE 83, FORMULA 20,
AND PAGE 84, THIRD FORMULA.
--PAULSON, AN APPROXIMATE NORMALIZATION
OF THE ANALYSIS OF VARIANCE DISTRIBUTION,
ANNALS OF MATHEMATICAL STATISTICS, 1942,
NUMBER 13, PAGES 233-135.
--SCHEFFE AND TUKEY, A FORMULA FOR SAMPLE SIZES
FOR POPULATION TOLERANCE LIMITS, 1944,
NUMBER 15, PAGE 217.

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UPDATED --AUGUST 1979.

```

58      C      IPR=6
59      C      CHECK THE INPUT ARGUMENTS FOR ERRORS
60      C
61      C
62      PPF=0.0
63      IF (NU1.LE.0) GO TO 10
64      IF (NU2.LE.0) GO TO 20
65      IF (P.LT.0.0.OR.P.GE.1.0) GO TO 30
66      GO TO 40
67      WRITE (IPR,60)
68      WRITE (IPR,90) NU1
69      PPF=0.0
70      RETURN
71      WRITE (IPR,70)
72      WRITE (IPR,90) NU2
73      PPF=0.0
74      RETURN
75      WRITE (IPR,50)
76      WRITE (IPR,80) P
77      PPF=0.0
78      RETURN
79      CONTINUE
80      FORMAT (1H ,113H***** FATAL ERROR--THE FIRST INPUT ARGUMENT TO THE
81      2E FPPF SUBROUTINE IS OUTSIDE THE ALLOWABLE (0,1) INTERVAL ***** FPPF0058
82      FORMAT (1H ,91H***** FATAL ERROR--THE SECOND INPUT ARGUMENT TO THE
83      2 FPPF SUBROUTINE IS NON-POSITIVE ***** FPPF0059
84      FORMAT (1H ,91H***** FATAL ERROR--THE THIRD INPUT ARGUMENT TO THE
85      2 FPDF SUBROUTINE IS NON-POSITIVE ***** FPPF0060
86      FORMAT (1H ,35H***** THE VALUE OF THE ARGUMENT IS ,E15.8,6H ***** FPPF0061
87      FORMAT (1H ,35H***** THE VALUE OF THE ARGUMENT IS ,I8,6H ***** FPPF0062
88      C-----START POINT-----
89      C
90      C      IBUG=0.0
91      C
92      TOL=0.000001
93      MAXIT=100
94      XMIN=0.0
95      XMAX=10.0**30
96      XLOW=XMIN
97      XUP=XMAX
98      C
99      ANU1=NU1
100     ANU2=NU2
101     C
102     EXPF=0.5*((1.0/ANU2)-(1.0/ANU1))
103     SDF=SQRT(0.5*((1.0/ANU2)+(1.0/ANU1)))
104     CALL NORPPF (P,ZN)
105     XN=EXPF+ZN*SDF
106     XMID=EXP(2.0*XN)
107     IF (IBUG.EQ.1) WRITE (6,100) XMID
108     FORMAT (1H ,7HXMID = ,E15.7)
109     C
110     IF (P.EQ.0.0) GO TO 110
111     GO TO 120
112     CONTINUE
113     PPF=XMIN
114     RETURN
115

```


116				FPPF0116
117				FPPF0117
118				FPPF0118
119				FPPF0119
120				FPPF0120
121				FPPF0121
122				FPPF0122
123				FPPF0123
124				FPPF0124
125				FPPF0125
126				FPPF0126
127				FPPF0127
128				FPPF0128
129				FPPF0129
130				FPPF0130
131				FPPF0131
132				FPPF0132
133				FPPF0133
134				FPPF0134
135				FPPF0135
136				FPPF0136
137				FPPF0137
138				FPPF0138
139				FPPF0139
140				FPPF0140
141				FPPF0141
142				FPPF0142
143				FPPF0143
144				FPPF0144
145				FPPF0145
146				FPPF0146
147				FPPF0147
148				FPPF0148
149				FPPF0149
150				FPPF0150
151				FPPF0151
152				FPPF0152
153				FPPF0153
154				FPPF0154
155				FPPF0155
156				FPPF0156
157				FPPF0157
158				FPPF0158
159				FPPF0159
160				FPPF0160
161				FPPF0161
162				FPPF0162
163				FPPF0163
164				FPPF0164
165				FPPF0165
166				FPPF0166
120		CONTINUE		
C		ICOUNT=0		
C		CONTINUE		
130		X=XMID		
		CALL FPDF (X,NU1,NU2,PCALC)		
		IF (PCALC.EQ.P) GO TO 190		
		IF (PCALC.GT.P) GO TO 160		
C		CONTINUE		
140		XLOW=XMID		
		X=XMID*2.0		
		IF (X.GE.XUP) GO TO 150		
		XMID=X		
		IF (IBUG.EQ.1) WRITE (6,100) XMID		
		CALL FPDF (X,NU1,NU2,PCALC)		
		IF (PCALC.EQ.P) GO TO 190		
		IF (PCALC.LT.P) GO TO 140		
		XUP=X		
		CONTINUE		
150		XMID=(XLOW+XUP)/2.0		
		IF (IBUG.EQ.1) WRITE (6,100) XMID		
		GO TO 180		
C		CONTINUE		
160		XUP=XMID		
		X=XMID/2.0		
		IF (X.LE.XLOW) GO TO 170		
		XMID=X		
		IF (IBUG.EQ.1) WRITE (6,100) XMID		
		CALL FPDF (X,NU1,NU2,PCALC)		
		IF (PCALC.EQ.P) GO TO 190		
		IF (PCALC.GT.P) GO TO 160		
		XLOW=X		
		CONTINUE		
170		XMID=(XLOW+XUP)/2.0		
		IF (IBUG.EQ.1) WRITE (6,100) XMID		
		GO TO 180		
C		CONTINUE		
180		XDEL=ABS(XMID-XLOW)		
		ICOUNT=ICOUNT+1		
		IF (XDEL.LT.TOL.OR.ICOUNT.GT.MAXIT) GO TO 190		
		GO TO 130		
C		CONTINUE		
190		PPF=XMID		
C		RETURN		
		END		

```

CPR*NS(1).GETX(2)
1
2
3
4
5
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9
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11
12
13
14
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17
18
19
20
21
22
23
24
25
26
27
28
29
30

SUBROUTINE GETX (XF,YF,NF,Y,L,M,X,I,KS,KL)
C-----
C  GETX  WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
C  DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
C  AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
C  FOR: THE INVERSE INTERPOLATION OF A CALIBRATION CURVE OR ITS
C  UPPER OR LOWER CONFIDENCE LIMIT WHEREBY AN X-VALUE IS
C  COMPUTED FOR A GIVEN Y-VALUE
C  SUBPROGRAMS CALLED: -NONE-
C  CURRENT VERSION COMPLETED JUNE 18, 1980
C-----
C  DIMENSION XF(NF), YF(NF)
10  IF (Y.LT.YF(L+1)) GO TO 20
    IF (L+1.EQ.NF) GO TO 30
    L=L+1
    GO TO 10
20  IF (L.EQ.0) GO TO 40
    C=(Y-YF(L))/(YF(L+1)-YF(L))
    X=C*(XF(L+1)-XF(L))+XF(L)
    I=1
    RETURN
30  X=XF(NF)
    I=(5+M)/2
    KL=KL+1
    RETURN
40  X=XF(1)
    I=(5-M)/2
    KS=KS+1
    RETURN
    END

```

GETX0001
 GETX0002
 GETX0003
 GETX0004
 GETX0005
 GETX0006
 GETX0007
 GETX0008
 GETX0009
 GETX0010
 GETX0011
 GETX0012
 GETX0013
 GETX0014
 GETX0015
 GETX0016
 GETX0017
 GETX0018
 GETX0019
 GETX0020
 GETX0021
 GETX0022
 GETX0023
 GETX0024
 GETX0025
 GETX0026
 GETX0027
 GETX0028
 GETX0029
 GETX0030

```

1 SUBROUTINE INTERV (XT,LXT,X,LEFT,MFLAG)
2 C FROM * A PRACTICAL GUIDE TO SPLINES * BY C. DE BOOR
3 COMPUTES LEFT = MAX( I , 1 .LE. I .LE. LXT .AND. XT(1) .LE. X ) .
4 C
5 C***** I N P U T *****
6 C XT....A REAL SEQUENCE, OF LENGTH LXT, ASSUMED TO BE NONDECREASING
7 C LXT....NUMBER OF TERMS IN THE SEQUENCE XT .
8 C X....THE POINT WHOSE LOCATION WITH RESPECT TO THE SEQUENCE XT IS
9 C TO BE DETERMINED.
10 C
11 C***** O U T P U T *****
12 C LEFT, MFLAG....BOTH INTEGERS, WHOSE VALUE IS
13 C
14 C 1 -1 IF X.LT. XT(1)
15 C I 0 IF XT(1) .LE. X.LT. XT(I+1)
16 C LXT 1 IF XT(LXT) .LE. X
17 C
18 IN PARTICULAR, MFLAG = 0 IS THE 'USUAL' CASE. MFLAG .NE. 0
19 INDICATES THAT X LIES OUTSIDE THE HALFOPEN INTERVAL
20 XT(1) .LE. Y .LT. XT(LXT) . THE ASYMMETRIC TREATMENT OF THE
21 INTERVAL IS DUE TO THE DECISION TO MAKE ALL PP FUNCTIONS CONT-
22 INUOUS FROM THE RIGHT.
23 C
24 C***** M E T H O D *****
25 C THE PROGRAM IS DESIGNED TO BE EFFICIENT IN THE COMMON SITUATION THAT
26 C IT IS CALLED REPEATEDLY, WITH X TAKEN FROM AN INCREASING OR DECREA-
27 C SING SEQUENCE. THIS WILL HAPPEN, E.G., WHEN A PP FUNCTION IS TO BE
28 C GRAPHED. THE FIRST GUESS FOR LEFT IS THEREFORE TAKEN TO BE THE VAL-
29 C UE RETURNED AT THE PREVIOUS CALL AND STORED IN THE L O C A L VARIA-
30 C BLE ILO . A FIRST CHECK ASCERTAINS THAT ILO .LT. LXT (THIS IS NEC-
31 C ESSARY SINCE THE PRESENT CALL MAY HAVE NOTHING TO DO WITH THE PREVI-
32 C OUS CALL). THEN, IF XT(ILO) .LE. X .LT. XT(ILO+1), WE SET LEFT =
33 C ILO AND ARE DONE AFTER JUST THREE COMPARISONS.
34 C OTHERWISE, WE REPEATEDLY DOUBLE THE DIFFERENCE ISTEP = IHI - ILO
35 C WHILE ALSO MOVING ILO AND IHI IN THE DIRECTION OF X, UNTIL
36 C XT(ILO) .LE. X .LT. XT(IHI),
37 C AFTER WHICH WE USE BISECTION TO GET, IN ADDITION, ILO+1 = IHI .
38 C LEFT = ILO IS THEN RETURNED.
39 C
40 INTEGER LEFT,LXT,MFLAG,IHI,ILO,ISTEP,MIDDLE
41 REAL X,XT(LXT)
42 DATA ILO /1/
43 SAVE ILO (A VALID FORTRAN STATEMENT IN THE NEW 1977 STANDARD)
44 IHI=ILO+1
45 IF (IHI.LT.LXT) GO TO 10
46 IF (X.GE.XT(LXT)) GO TO 110
47 IF (LXT.LE.1) GO TO 90
48 ILO=LXT-1
49 IHI=LXT
50
51 10 IF (X.GE.XT(IHI)) GO TO 40
52 IF (X.GE.XT(ILO)) GO TO 100
53 C
54 C ***** NOW X .LT. XT(ILO) . DECREASE ILO TO CAPTURE X .
55 ISTEP=1
56 IHI=ILO
57 ILO=IHI-ISTEP

```



```

58 INTERV58
59 INTERV59
60 INTERV60
61 INTERV61
62 INTERV62
63 INTERV63
64 INTERV64
65 INTERV65
66 INTERV66
67 INTERV67
68 INTERV68
69 INTERV69
70 INTERV70
71 INTERV71
72 INTERV72
73 INTERV73
74 INTERV74
75 INTERV75
76 INTERV76
77 INTERV77
78 INTERV78
79 INTERV79
80 INTERV80
81 INTERV81
82 INTERV82
83 INTERV83
84 INTERV84
85 INTERV85
86 INTERV86
87 INTERV87
88 INTERV88
89 INTERV89
90 INTERV90
91 INTERV91
92 INTERV92
93 INTERV93
94 INTERV94
95 INTERV95

IF (ILO.LE.1) GO TO 30
IF (X.GE.XT(ILO)) GO TO 70
ISTEP=ISTEP*2
GO TO 20
30 ILO=1
IF (X.LT.XT(1)) GO TO 90
GO TO 70
C ***** NOW X .GE. XT(IHI) . INCREASE IHI TO CAPTURE X .
40 ISTEP=1
41 ILO=IHI
42 IHI=ILO+ISTEP
43 IF (IHI.GE.LXT) GO TO 60
44 IF (X.LT.XT(IHI)) GO TO 70
45 ISTEP=ISTEP*2
46 GO TO 50
47 IF (X.GE.XT(LXT)) GO TO 110
48 IHI=LXT
C ***** NOW XT(ILO) .LE. X .LT. XT(IHI) . NARROW THE INTERVAL.
49 MIDDLE=(ILO+IHI)/2
50 IF (MIDDLE.EQ.ILO) GO TO 100
51 NOTE. IT IS ASSUMED THAT MIDDLE = ILO IN CASE IHI = ILO+1 .
52 IF (X.LT.XT(MIDDLE)) GO TO 80
53 ILO=MIDDLE
54 GO TO 70
55 IHI=MIDDLE
56 GO TO 70
80 C**** SET OUTPUT AND RETURN.
81 MFLAG=-1
82 LEFT=1
83 RETURN
84 MFLAG=0
85 LEFT=ILO
86 RETURN
87 MFLAG=1
88 LEFT=LXT
89 RETURN
90 END
100
110

```

```

CPR*NS(1).L2APPR(1)
1 SUBROUTINE L2APPR (T,N,K,Q,DIAG,BCOEF,KMX,NPK,NTAU,TAU,GTAU,
2 WEIGHT)
3
4 C
5 INTEGER N,K,KMX,NPK,NTAU
6 REAL Q(KMX,N)
7 REAL T(NPK),DIAG(N),BCOEF(N),TAU(NTAU),GTAU(NTAU),WEIGHT(NTAU)
8
9 C
10 CONSTRUCTS THE (WEIGHTED DISCRETE) L2-APPROXIMATION BY SPLINES OF ORDER
11 K WITH KNOT SEQUENCE T(1), ..., T(N+K) TO GIVEN DATA POINTS
12 C (TAU(1),GTAU(1)), I=1,...,NTAU. THE B-SPLINE COEFFICIENTS
13 C B O E F OF THE APPROXIMATING SPLINE ARE DETERMINED FROM THE
14 C NORMAL EQUATIONS USING CHOLESKY'S METHOD.
15
16 C
17 ON INPUT.
18
19 C
20 T(*)
21 IS AN ARRAY OF SIZE AT LEAST NPK = N + K AND HOLDS
22 THE KNOT SEQUENCE IN T(1) . . . T(NPK)
23
24 C
25 N
26 IS THE DIMENSION OF THE SPACE OF SPLINES OF ORDER
27 WITH KNOTS T.
28
29 C
30 K
31 IS THE ORDER OF THE SPLINES = DEGREE + 1
32
33 C
34 Q(*,*)
35 IS A WORK ARRAY WITH ROW DIMENSION KMX AND COLUMN
36 DIMENSION AT LEAST N.
37
38 C
39 DIAG(*)
40 IS A WORK ARRAY OF SIZE AT LEAST N.
41
42 C
43 KMX
44 IS THE ROW DIMENSION OF Q.
45
46 C
47 NPK
48 IS N + K.
49
50 C
51 NTAU
52 IS THE NUMBER OF DATA POINTS.
53
54 C
55 TAU(*)
56 IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
57 THE ABSISSAS OF THE DATA POINTS TO BE FITTED IN
58 TAU(1) . . . TAU(NTAU).
59
60 C
61 GTAU(*)
62 IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
63 THE ORDINATES OF THE DATA POINTS TO BE FITTED IN
64 GTAU(1) . . . GTAU(NTAU).
65
66 C
67 WEIGHT(*)
68 IS AN ARRAY OF SIZE AT LEAST NTAU WHICH CONTAINS
69 THE CORRESPONDING WEIGHTS TO BE APPLIED TO THE
70 DATA POINTS WHEN FITTING IN WEIGHT(1) . . .
71 WEIGHT(NTAU).
72
73 C
74 ON OUTPUT.
75
76 C
77 Q(*,*)
78 CONTAINS THE K LOWER DIAGONALS OF THE CHOLESKY
79 FACTOR OF THE GRAMIAN MATRIX C IN ITS FIRST K ROWS.
80
81 C
82 DIAG(*)
83 CONTAINS LITTLE OF IMPORTANCE.
84
85 C
86 BCOEF(*)
87 IS AN ARRAY OF SIZE AT LEAST N WHICH CONTAINS THE
88 B-SPLINE COEFFICIENTS OF THE L2 APPROXIMATION IN
89 BCOEF(1) . . . BCOEF(N).
90
91 C

```

```

58 C
59 C
60 C
61 C ***** M E T H O D *****
62 C THE B-SPLINE COEFFICIENTS OF THE L2-APPR. ARE DETERMINED AS THE SOL-
63 C UTION OF THE NORMAL EQUATIONS
64 C SUM ( (B(I),B(J))*BCOEF(J) : J=1,...,N) = (B(I),G),
65 C I = 1, ..., N .
66 C HERE, B(I) DENOTES THE I-TH B-SPLINE, G DENOTES THE FUNCTION TO
67 C BE APPROXIMATED, AND THE I N N E R P R O D U C T OF TWO FUNCT-
68 C IONS F AND G IS GIVEN BY
69 C (F,G) := SUM ( F(TAU(I))*G(TAU(I))*WEIGHT(I) : I=1,...,NTAU) .
70 C THE ARRAYS T A U AND W E I G H T ARE GIVEN IN COMMON BLOCK
71 C D A T A , AS IS THE ARRAY G T A U CONTAINING THE SEQUENCE
72 C G(TAU(I)), I=1,...,NTAU.
73 C THE RELEVANT FUNCTION VALUES OF THE B-SPLINES B(I), I=1,...,N, ARE
74 C SUPPLIED BY THE SUBPROGRAM B S P L V B .
75 C THE COEFF.MATRIX C, WITH
76 C C(I,J) := (B(I),B(J)), I,J=1,...,N,
77 C OF THE NORMAL EQUATIONS IS SYMMETRIC AND (2*K-1)-BANDED, THEREFORE
78 C CAN BE SPECIFIED BY GIVING ITS K BANDS AT OR BELOW THE DIAGONAL. FOR
79 C I=1,...,N, WE STORE
80 C (B(I),B(J)) = C(I,J) IN Q(I-J+1,J), J=1,...,MIN0(I+K-1,N)
81 C AND THE RIGHT SIDE
82 C (B(I),G) IN BCOEF(I) .
83 C SINCE B-SPLINE VALUES ARE MOST EFFICIENTLY GENERATED BY FINDING SIM-
84 C ULTANEOUSLY THE VALUE OF E V E R Y NONZERO B-SPLINE AT ONE POINT,
85 C THE ENTRIES OF C (I.E., OF Q), ARE GENERATED BY COMPUTING, FOR
86 C EACH LL, ALL THE TERMS INVOLVING TAU(LL) SIMULTANEOUSLY AND ADDING
87 C THEM TO ALL RELEVANT ENTRIES.
88 C
89 C ADDITIONAL ROUTINES REQUIRED.
90 C
91 C BSPLVB BCFAC BCHSLV
92 C
93 C MODIFICATION BY.
94 C
95 C MARTIN CORDES
96 C CENTER FOR APPLIED MATHEMATICS, NBS
97 C VERSION 1
98 C OCT 1979
99 C
100 C -----
101 C
102 C REAL BIATX(20)
103 C REAL DW
104 C INTEGER I,J,JJ,LEFT,LEFTMK,LL,MM
105 C FORMAT (/5X,5H<<<<< 14,1X,22HB-SPLINE COEFFICIENTS ,
106 C 2 14HCOMPUTED >>>>>)
107 C
108 C DO 20 J=1,N
109 C BCOEF(J)=0.
110 C DO 20 I=1,K
111 C Q(I,J)=0.
112 C LEFT=K
113 C LEFTMK=0
114 C DO 50 LL=1,NTAU
115 C LOCATE L E F T S.T. TAU(LL) IN (T(LEFT),T(LEFT+1)) L2APP115

```



```

30  IF (LEFT.EQ.N) GO TO 40
    IF (TAU(LL).LT.T(LEFT+1)) GO TO 40
    LEFT=LEFT+1
    LEFTMK=LEFTMK+1
    GO TO 30
40  CALL BSPLVB (T,K,1,TAU(LL),LEFT,BIATX)
    BIATX(MM) CONTAINS THE VALUE OF B(LEFT-K+MM AT TAU(LL).
    HENCE, WITH DW := BIATX(MM)*WEIGHT(LL), THE NUMBER DW*CTAU(LL)
    IS A SUMMAND IN THE INNER PRODUCT
    (B(LEFT-K+MM), C) WHICH GOES INTO BCOEF(LEFT-K+MM)
    AND THE NUMBER BIATX(JJ)*DW IS A SUMMAND IN THE INNER PRODUCT
    (B(LEFT-K+JJ), B(LEFT-K+MM)), INTO Q(JJ-MM+1,LEFT-K+MM)
    SINCE (LEFT-K+JJ) - (LEFT-K+MM) + 1 = JJ - MM + 1.
    DO 50 MM=1,K
    DW=BIATX(MM)*WEIGHT(LL)
    J=LEFTMK+MM
    BCOEF(J)=DW*CTAU(LL)+BCOEF(J)
    I=1
    DO 50 JJ=MM,K
    Q(I,J)=BIATX(JJ)*DW+Q(I,J)
    I=I+1
50  CONSTRUCT CHOLESKY FACTORIZATION FOR C IN Q, THEN USE
    IT TO SOLVE THE NORMAL EQUATIONS
    C*X = BCOEF
    FOR X, AND STORE X IN BCOEF.
    CALL BCFAC (Q,KMX,K,N,DIAG)
    CALL BCBSLV (Q,KMX,K,N,BCOEF)
    WRITE (6,10) N
    RETURN
    END

```

```

CPR*NS(1).NORCDF(1)
1 SUBROUTINE NORCDF (X,CDF)
2
3 C
4 C
5 C
6 C
7 C
8 C
9 C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
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56 C

PURPOSE--THIS SUBROUTINE COMPUTES THE CUMULATIVE DISTRIBUTION
FUNCTION VALUE FOR THE NORMAL (GAUSSIAN)
DISTRIBUTION WITH MEAN = 0 AND STANDARD DEVIATION = 1.
THIS DISTRIBUTION IS DEFINED FOR ALL X AND HAS
THE PROBABILITY DENSITY FUNCTION
 $F(X) = (1/\sqrt{2\pi}) * \exp(-X^2/2)$ .
INPUT ARGUMENTS--X = THE SINGLE PRECISION VALUE AT
WHICH THE CUMULATIVE DISTRIBUTION
FUNCTION IS TO BE EVALUATED.
OUTPUT ARGUMENTS--CDF = THE SINGLE PRECISION CUMULATIVE
DISTRIBUTION FUNCTION VALUE.
OUTPUT--THE SINGLE PRECISION CUMULATIVE DISTRIBUTION
FUNCTION VALUE CDF.
PRINTING--NONE.
RESTRICTIONS--NONE.
OTHER DATAPAC SUBROUTINES NEEDED--NONE.
FORTRAN LIBRARY SUBROUTINES NEEDED--EXP.
MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.
LANGUAGE--ANSI FORTRAN.
REFERENCES--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
SERIES 55, 1964, PAGE 932, FORMULA 26.2.17.
--JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE
DISTRIBUTIONS--1, 1970, PAGES 40-111.
WRITTEN BY--JAMES J. FILLIBEN
STATISTICAL ENGINEERING LABORATORY (205.03)
NATIONAL BUREAU OF STANDARDS
WASHINGTON, D. C. 20234
PHONE: 301-921-2315
ORIGINAL VERSION--JUNE 1972.
UPDATED --SEPTEMBER 1975.
UPDATED --NOVEMBER 1975.

DATA B1,B2,B3,B4,B5,P /-.319381530,-0.356563782,1.781477937,
2 -1.821255978,1.330274429,.2316419/

IPR=6

CHECK THE INPUT ARGUMENTS FOR ERRORS.
NO INPUT ARGUMENT ERRORS POSSIBLE
FOR THIS DISTRIBUTION.

-----START POINT-----
Z=X
IF (X.LT.0.0) Z=-Z
T=1.0/(1.0+P*Z)
CDF=1.0-((0.39894228040143)*EXP(-0.5*Z*Z))*(B1*T+B2*T**2+B3*T**3+B4*T**4+B5*T**5)
IF (X.LT.0.0) CDF=1.0-CDF

RETURN
END

```

SUBROUTINE NORPPF (P,PPF)

PURPOSE--THIS SUBROUTINE COMPUTES THE PERCENT POINT
FUNCTION VALUE FOR THE NORMAL (GAUSSIAN)
DISTRIBUTION WITH MEAN = 0 AND STANDARD DEVIATION = 1.

THIS DISTRIBUTION IS DEFINED FOR ALL X AND HAS
THE PROBABILITY DENSITY FUNCTION

$$f(x) = (1/\sqrt{2\pi}) * \exp(-x^2/2).$$

NOTE THAT THE PERCENT POINT FUNCTION OF A DISTRIBUTION
IS IDENTICALLY THE SAME AS THE INVERSE CUMULATIVE
DISTRIBUTION FUNCTION OF THE DISTRIBUTION.

INPUT ARGUMENTS--P = THE SINGLE PRECISION VALUE
(BETWEEN 0.0 AND 1.0)

AT WHICH THE PERCENT POINT
FUNCTION IS TO BE EVALUATED.

OUTPUT ARGUMENTS--PPF = THE SINGLE PRECISION PERCENT
POINT FUNCTION VALUE.

OUTPUT--THE SINGLE PRECISION PERCENT POINT
FUNCTION VALUE PPF.

PRINTING--NONE UNLESS AN INPUT ARGUMENT ERROR CONDITION EXISTS.
RESTRICTIONS--P SHOULD BE BETWEEN 0.0 AND 1.0, EXCLUSIVELY.

OTHER DATAPAC SUBROUTINES NEEDED--NONE.

FORTRAN LIBRARY SUBROUTINES NEEDED--SQRT, ALOG.

MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.

LANGUAGE--ANSI FORTRAN.

REFERENCES--ODEH AND EVANS, THE PERCENTAGE POINTS
OF THE NORMAL DISTRIBUTION, ALGORITHM 70,
APPLIED STATISTICS, 1974, PAGES 96-97.

--EVANS, ALGORITHMS FOR MINIMAL DEGREE

POLYNOMIAL AND RATIONAL APPROXIMATION,

M. SC. THESIS, 1972, UNIVERSITY

OF VICTORIA, B. C., CANADA.

--HASTINGS, APPROXIMATIONS FOR DIGITAL

COMPUTERS, 1955, PAGES 113, 191, 192.

--NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS

SERIES 55, 1964, PAGE 933, FORMULA 26.2.23.

--FILLIBEN, SIMPLE AND ROBUST LINEAR ESTIMATION

OF THE LOCATION PARAMETER OF A SYMMETRIC

DISTRIBUTION (UNPUBLISHED PH.D. DISSERTATION,

PRINCETON UNIVERSITY), 1969, PAGES 21-44, 229-231.

--FILLIBEN, 'THE PERCENT POINT FUNCTION',

(UNPUBLISHED MANUSCRIPT), 1970, PAGES 28-31.

--JOHNSON AND KOTZ, CONTINUOUS UNIVARIATE

DISTRIBUTIONS--1, 1970, PAGES 40-111.

--THE KELLEY STATISTICAL TABLES, 1948.

--OWEN, HANDBOOK OF STATISTICAL TABLES,

1962, PAGES 3-16.

--PEARSON AND HARTLEY, BIOMETRIKA TABLES

FOR STATISTICIANS, VOLUME 1, 1954,

PAGES 104-113.

COMMENTS--THE CODING AS PRESENTED BELOW

IS ESSENTIALLY IDENTICAL TO THAT

PRESENTED BY ODEH AND EVANS

AS ALGORITHM 70 OF APPLIED STATISTICS.

THE PRESENT AUTHOR HAS MODIFIED THE

ORIGINAL ODEH AND EVANS CODE WITH ONLY

MINOR STYLISTIC CHANGES.

NORPP001
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NORPP003
NORPP004
NORPP005
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--AS POINTED OUT BY ODEH AND EVANS
IN APPLIED STATISTICS,
THEIR ALGORITHM REPRESENTS A
SUBSTANTIAL IMPROVEMENT OVER THE
PREVIOUSLY EMPLOYED
HASTINGS APPROXIMATION FOR THE
NORMAL PERCENT POINT FUNCTION--
THE ACCURACY OF APPROXIMATION
BEING IMPROVED FROM 4.5*(10**-4)
TO 1.5*(10**-8).
WRITTEN BY--JAMES J. FILLIBEN
STATISTICAL ENGINEERING LABORATORY (205.03)
NATIONAL BUREAU OF STANDARDS
WASHINGTON, D. C. 20234
PHONE: 301-921-2315
ORIGINAL VERSION--JUNE 1972.
UPDATED --SEPTEMBER 1975.
UPDATED --NOVEMBER 1975.
UPDATED --OCTOBER 1976.
-----
DATA P0,P1,P2,P3,P4 /-.322232431088,-1.0,-.342242088547,
2 -.204231210245E-1,-.453642210148E-4/
DATA Q0,Q1,Q2,Q3,Q4 / .993484626060E-1,.588581570495,.531103462366,
2 .103537752850,.38560700634E-2/
IPR=6
CHECK THE INPUT ARGUMENTS FOR ERRORS
IF (P.LE.0.0.OR.P.GE.1.0) GO TO 10
GO TO 20
WRITE (IPR,30)
WRITE (IPR,40) P
RETURN
CONTINUE
FORMAT (1H,115H***** FATAL ERROR--THE FIRST INPUT ARGUMENT TO THNORPP095
2E NORPPF SUBROUTINE IS OUTSIDE THE ALLOWABLE (0,1) INTERVAL ***** NORPP096
FORMAT (1H,35H***** THE VALUE OF THE ARGUMENT IS ,E15.8,6H ***** NORPP097
C
C-----START POINT-----
C
IF (P.NE.0.5) GO TO 50
PPF=0.0
RETURN
R=P
IF (P.GT.0.5) R=1.0-R
T=SQR((-2.0*ALOG(R))
ANUM=((T*P4+P3)*T+P2)*T+P1)*T+P0)
ADEN=((T*Q4+Q3)*T+Q2)*T+Q1)*T+Q0)
PPF=T+(ANUM/ADEN)
IF (P.LT.0.5) PPF=-PPF
RETURN
END

```

```

CPR*NS(1).PLOT(2)
SUBROUTINE PLOT( Y,X,CHAR,N,ITYPE)
PURPOSE--THIS SUBROUTINE YIELDS A ONE-PAGE PRINTER PLOT
OF Y(I) VERSUS X(I) WITH SPECIAL PLOTTING
CHARACTERS.
THIS 'SPECIAL PLOTTING CHARACTER' CAPABILITY
ALLOWS THE DATA ANALYST TO INCORPORATE INFORMATION
FROM A THIRD VARIABLE (ASIDE FROM Y AND X) INTO
THE PLOT.
THE PLOT CHARACTER USED AT THE I-TH PLOTTING
POSITION (THAT IS, AT THE COORDINATE (X(I),Y(I)))
WILL BE
1 IF CHAR(I) IS BETWEEN 0.5 AND 1.5
2 IF CHAR(I) IS BETWEEN 1.5 AND 2.5
.
.
9 IF CHAR(I) IS BETWEEN 8.5 AND 9.5
. IF CHAR(I) IS BETWEEN 9.5 AND 10.5
A IF CHAR(I) IS BETWEEN 10.5 AND 11.5
B IF CHAR(I) IS BETWEEN 11.5 AND 12.5
C IF CHAR(I) IS BETWEEN 12.5 AND 13.5
.
.
W IF CHAR(I) IS BETWEEN 32.5 AND 33.5
X IF CHAR(I) IS BETWEEN 33.5 AND 34.5
Y IF CHAR(I) IS BETWEEN 34.5 AND 35.5
Z IF CHAR(I) IS BETWEEN 35.5 AND 36.5
X IF CHAR(I) IS ANY VALUE OUTSIDE THE RANGE
0.5 TO 36.5.
INPUT ARGUMENTS--Y = THE SINGLE PRECISION VECTOR OF
(UNSORTED OR SORTED) OBSERVATIONS
TO BE PLOTTED VERTICALLY.
--X = THE SINGLE PRECISION VECTOR OF
(UNSORTED OR SORTED) OBSERVATIONS
TO BE PLOTTED HORIZONTALLY.
--CHAR = THE SINGLE PRECISION VECTOR OF
OBSERVATIONS WHICH CONTROL THE
VALUE OF EACH INDIVIDUAL PLOT
CHARACTER.
--N = THE INTEGER NUMBER OF OBSERVATIONS
IN THE VECTOR Y.
OUTPUT--A ONE-PAGE PRINTER PLOT OF Y(I) VERSUS X(I)
WITH SPECIAL PLOT CHARACTERS.
PRINTING--YES.
RESTRICTIONS--THERE IS NO RESTRICTION ON THE MAXIMUM VALUE
OF N FOR THIS SUBROUTINE.
OTHER DATAPAC SUBROUTINES NEEDED--NONE.
FORTRAN LIBRARY SUBROUTINES NEEDED--NONE.
MODE OF INTERNAL OPERATIONS--SINGLE PRECISION.
LANGUAGE--ANSI FORTRAN.
COMMENT--VALUES IN THE VERTICAL AXIS VECTOR (Y),
THE HORIZONTAL AXIS VECTOR (X),
OR THE PLOT CHARACTER VECTOR (CHAR) WHICH ARE
EQUAL TO OR IN EXCESS OF 10.0**10 WILL NOT BE
PLOTTED.

```


58 C THIS CONVENTION GREATLY SIMPLIFIES THE PROBLEM
59 C OF PLOTTING WHEN SOME ELEMENTS IN THE VECTOR Y
60 C (OR X, OR CHAR) ARE 'MISSING DATA', OR WHEN WE PURPOSELY
61 C WANT TO IGNORE CERTAIN ELEMENTS IN THE VECTOR Y
62 C (OR X, OR CHAR) FOR PLOTTING PURPOSES (THAT IS, WE DO NOT
63 C WANT CERTAIN ELEMENTS IN Y (OR X, OR CHAR) TO BE
64 C PLOTTED).
65 C TO CAUSE SPECIFIC ELEMENTS IN Y (OR X, OR CHAR) TO BE
66 C IGNORED, WE REPLACE THE ELEMENTS BEFOREHAND
67 C (BY, FOR EXAMPLE, USE OF THE REPLAC SUBROUTINE)
68 C BY SOME LARGE VALUE (LIKE, SAY, 10.0**10) AND
69 C THEY WILL SUBSEQUENTLY BE IGNORED IN THE PLOT
70 C SUBROUTINE.
71 C REFERENCES--FILLIBEN, 'STATISTICAL ANALYSIS OF INTERLAB
72 C FATIGUE TIME DATA', UNPUBLISHED MANUSCRIPT
73 C (AVAILABLE FROM AUTHOR)
74 C PRESENTED AT THE 'COMPUTER-ASSISTED DATA
75 C ANALYSIS' SESSION AT THE NATIONAL MEETING
76 C OF THE AMERICAN STATISTICAL ASSOCIATION,
77 C NEW YORK CITY, DECEMBER 27-30, 1973.
78 C WRITTEN BY--JAMES J. FILLIBEN
79 C STATISTICAL ENGINEERING LABORATORY (205.03)
80 C NATIONAL BUREAU OF STANDARDS
81 C WASHINGTON, D. C. 20234
82 C PHONE--301-921-2315
83 C ORIGINAL VERSION--OCTOBER 1974.
84 C UPDATED --NOVEMBER 1974.
85 C UPDATED --JANUARY 1975.
86 C UPDATED --JULY 1975.
87 C UPDATED --SEPTEMBER 1975.
88 C UPDATED --OCTOBER 1975.
89 C UPDATED --NOVEMBER 1975.
90 C UPDATED --FEBRUARY 1976.
91 C UPDATED --FEBRUARY 1977.
92 C MINOR UPDATES --APRIL 1980 BY CHARLES P. REEVE.
93 C
94 C
95 C
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 PLOT115

DATA SBNAME(1), SBNAME(2), SBNAME(3), SBNAME(4), SBNAME(5), SBNAME(6),
 2 ALPHA1(1), ALPHA1(2), ALPHA1(3), ALPHA1(4), ALPHA1(5), ALPHA1(6),
 3 ALPHA2(1), ALPHA2(2), ALPHA2(3), ALPHA2(4), ALPHA2(5), ALPHA2(6),
 4 ALPHA3(1), ALPHA3(2), ALPHA3(3), ALPHA3(4), ALPHA3(5), ALPHA3(6),
 5 ALPHA4(1), ALPHA4(2), ALPHA4(3), ALPHA4(4), ALPHA4(5), ALPHA4(6) /1HP,
 6 1HL, 1HO, 1HT, 1HC, 1H, 1HF, 1HI, 1HR, 1HS, 1HT, 1H, 1HS, 1HE, 1HG, 1HO, 1HN,
 7 1HD, 1HT, 1HH, 1HI, 1HR, 1HD, 1H, 1HF, 1HO, 1HU, 1HR, 1HT, 1HH/
 DATA BLANK, HYPHEN, ALPHA1, ALPHAX /1H, 1H-, 1H1, 1HX/
 DATA ALPHAM, ALPHAA, ALPHAD, ALPHAN, EQUAL /1HM, 1HA, 1HD, 1HN, 1H=/
 DATA IPLOT(1), IPLOT(2), IPLOT(3), IPLOT(4), IPLOT(5), IPLOT(6),
 2 IPLOT(7), IPLOT(8), IPLOT(9), IPLOT(10), IPLOT(11), IPLOT(12),
 3 IPLOT(13), IPLOT(14), IPLOT(15), IPLOT(16), IPLOT(17), IPLOT(18),
 4, IPLOT(19), IPLOT(20), IPLOT(21), IPLOT(22), IPLOT(23), IPLOT(24) PLOT115

INTEGER SBNAME(6)
 INTEGER ALPHA1(6), ALPHA2(6), ALPHA3(6), ALPHA4(6)
 INTEGER BLANK, HYPHEN, ALPHA1, ALPHAX
 INTEGER ALPHAM, ALPHAA, ALPHAD, ALPHAN, EQUAL
 DIMENSION Y(1), X(1), CHAR(1), YLAB(11), IPLOT(37)
 COMMON /BLOCK1/ IGRAPH(55,130)


```

174      WRITE (IPR,200)
175      WRITE (IPR,220)
176      WRITE (IPR,230)      (ALPHA3(L), L=1,6), (SBNAME(L), L=1,6)
177      WRITE (IPR,280)      HOLD
178      WRITE (IPR,200)
179      CONTINUE
180
181      DO 110 I=1,N
182      IF (Y(I).LT.CUTOFF) GO TO 120
183      CONTINUE
184      WRITE (IPR,200)
185      WRITE (IPR,210)
186      WRITE (IPR,230)      (ALPHA1(L), L=1,6), (SBNAME(L), L=1,6)
187      WRITE (IPR,290)      CUTOFF
188      WRITE (IPR,300)
189      WRITE (IPR,200)
190      RETURN
191
192      CONTINUE
193      DO 130 I=1,N
194      IF (X(I).LT.CUTOFF) GO TO 140
195      CONTINUE
196      WRITE (IPR,200)
197      WRITE (IPR,210)
198      WRITE (IPR,230)      (ALPHA2(L), L=1,6), (SBNAME(L), L=1,6)
199      WRITE (IPR,290)
200      WRITE (IPR,300)      CUTOFF
201      WRITE (IPR,200)
202      RETURN
203
204      CONTINUE
205      DO 150 I=1,N
206      IF (CHAR(I).LT.CUTOFF) GO TO 160
207      CONTINUE
208      WRITE (IPR,200)
209      WRITE (IPR,210)
210      WRITE (IPR,230)      (ALPHA3(L), L=1,6), (SBNAME(L), L=1,6)
211      WRITE (IPR,290)      CUTOFF
212      WRITE (IPR,300)
213      RETURN
214
215      CONTINUE
216      N2=0
217      DO 180 I=1,N
218      IF (Y(I).LT.CUTOFF.AND.X(I).LT.CUTOFF.AND.CHAR(I).LT.CUTOFF) GO TO 170
219      GO TO 180
220      N2=N2+1
221      IF (N2.GE.2) GO TO 190
222      CONTINUE
223      WRITE (IPR,200)
224      WRITE (IPR,210)
225      WRITE (IPR,240)      (ALPHA1(L), L=1,6), (ALPHA2(L), L=1,6), (ALPHA3(L), L=1,6)
226      WRITE (IPR,250)      (SBNAME(L), L=1,6)
227      WRITE (IPR,310)
228      WRITE (IPR,320)      N2
229      WRITE (IPR,200)
230      RETURN
231

```

```

190 CONTINUE
C
200 FORMAT (1H,50H*****FATAL ERROR*****),
2 20H*****FATAL FATAL ERROR*****
FORMAT (1H,50H
FORMAT (1H,50H NON-FATAL DIAGNOSTIC
FORMAT (1H,4THE,6A1,23H INPUT ARGUMENT TO THE,6A1,
2 11H SUBROUTINE)
FORMAT (1H,4THE,6A1,2H,6A1,6H,AND,6A1)
FORMAT (1H,23HINPUT ARGUMENTS TO THE,6A1,11H SUBROUTINE)
FORMAT (1H,30HIS NON-NEGATIVE (WITH VALUE =,18,1H)
FORMAT (1H,15HHAS THE VALUE 1)
FORMAT (1H,19HHAS ALL ELEMENTS =,E15.8)
FORMAT (1H,40HHAS ALL ELEMENTS IN EXCESS OF THE CUTOFF)
FORMAT (1H,9HVALUE OF,E15.8)
FORMAT (1H,39HARE SUCH THAT TOO MANY POINTS HAVE BEEN,
2 24H EXCLUDED FROM THE PLOT.)
FORMAT (1H,5HONLY,13,31H POINTS ARE LEFT TO BE PLOTTED.)
C
C-----START POINT-----C-----
C
C DETERMINE THE VALUES TO BE LISTED ON THE LEFT VERTICAL AXIS
C
DO 330 I=1,N
IF (Y(I).GE.CUTOFF) GO TO 330
IF (X(I).GE.CUTOFF) GO TO 330
IF (CHAR(I).GE.CUTOFF) GO TO 330
YMIN=Y(I)
YMAX=Y(I)
GO TO 340
CONTINUE
DO 350 I=1,N
IF (Y(I).GE.CUTOFF) GO TO 350
IF (X(I).GE.CUTOFF) GO TO 350
IF (CHAR(I).GE.CUTOFF) GO TO 350
IF (Y(I).LT.YMIN) YMIN=Y(I)
IF (Y(I).GT.YMAX) YMAX=Y(I)
CONTINUE
DO 360 I=1,9
AIM1=I-1
YLABE(I)=YMAX-(AIM1/8.0)*(YMAX-YMIN)
CONTINUE
C
C DETERMINE THE VALUES TO BE LISTED ON THE BOTTOM HORIZONTAL AXIS
C
C DETERMINE XMIN, XMAX, XMID, X25 (=THE 25% POINT), AND
C X75 (=THE 75% POINT)
C
DO 370 I=1,N
IF (Y(I).GE.CUTOFF) GO TO 370
IF (X(I).GE.CUTOFF) GO TO 370
IF (CHAR(I).GE.CUTOFF) GO TO 370
XMIN=X(I)
XMAX=X(I)
GO TO 380
CONTINUE
DO 390 I=1,N
IF (Y(I).GE.CUTOFF) GO TO 390
IF (X(I).GE.CUTOFF) GO TO 390

```


290	IF (CHAR(1),GE,CUTOFF) GO TO 390	PLOT3290
291	IF (X(1),LT,XMIN) XMIN=X(1)	PLOT3291
292	IF (X(1),GT,XMAX) XMAX=X(1)	PLOT3292
293	CONTINUE	PLOT3293
294	XMIN=(XMIN+XMAX)/2.0	PLOT3294
295	X25=0.75*XMIN+0.25*XMAX	PLOT3295
296	X75=0.25*XMIN+0.75*XMAX	PLOT3296
297		PLOT3297
298	BLANK OUT THE GRAPH	PLOT3298
299		PLOT3299
300	DO 410 I=1,45	PLOT3300
301	DO 400 J=1,109	PLOT3301
302	IGRAPH(I,J)=BLANK	PLOT3302
303	CONTINUE	PLOT3303
304	CONTINUE	PLOT3304
305		PLOT3305
306	PRODUCE THE VERTICAL AXES	PLOT3306
307		PLOT3307
308	DO 420 I=3,43	PLOT3308
309	IGRAPH(I,5)=ALPHAI	PLOT3309
310	IGRAPH(I,109)=ALPHAI	PLOT3310
311	CONTINUE	PLOT3311
312	DO 430 I=3,43,5	PLOT3312
313	IGRAPH(I,5)=HYPHEN	PLOT3313
314	IGRAPH(I,109)=HYPHEN	PLOT3314
315	CONTINUE	PLOT3315
316	IGRAPH(3,1)=EQUAL	PLOT3316
317	IGRAPH(3,2)=ALPHAM	PLOT3317
318	IGRAPH(3,3)=ALPHAA	PLOT3318
319	IGRAPH(3,4)=ALPHAX	PLOT3319
320	IGRAPH(23,1)=EQUAL	PLOT3320
321	IGRAPH(23,2)=ALPHAM	PLOT3321
322	IGRAPH(23,3)=ALPHAI	PLOT3322
323	IGRAPH(23,4)=ALPHAD	PLOT3323
324	IGRAPH(43,1)=EQUAL	PLOT3324
325	IGRAPH(43,2)=ALPHAM	PLOT3325
326	IGRAPH(43,3)=ALPHAI	PLOT3326
327	IGRAPH(43,4)=ALPHAN	PLOT3327
328	PRODUCE THE HORIZONTAL AXES	PLOT3328
329		PLOT3329
330		PLOT3330
331	DO 440 J=7,107	PLOT3331
332	IGRAPH(1,J)=HYPHEN	PLOT3332
333	IGRAPH(45,J)=HYPHEN	PLOT3333
334	CONTINUE	PLOT3334
335	DO 450 J=7,107,25	PLOT3335
336	IGRAPH(1,J)=ALPHAI	PLOT3336
337	IGRAPH(45,J)=ALPHAI	PLOT3337
338	CONTINUE	PLOT3338
339	DO 460 J=20,107,25	PLOT3339
340	IGRAPH(1,J)=ALPHAI	PLOT3340
341	IGRAPH(45,J)=ALPHAI	PLOT3341
342	CONTINUE	PLOT3342
343		PLOT3343
344	DETERMINE THE (X,Y) PLOT POSITIONS	PLOT3344
345	RATIOY=40.0/(YMAX-YMIN)	PLOT3345
346	RATIOX=100.0/(XMAX-XMIN)	PLOT3346
347		PLOT3347

```

348 DO 470 I=1,N
349 IF (Y(I).GE.CUTOFF) GO TO 470
350 IF (X(I).GE.CUTOFF) GO TO 470
351 IF (CHAR(I).GE.CUTOFF) GO TO 470
352 MX=RATIOX*(X(I)-XMIN)+0.5
353 MY=RATIOY*(Y(I)-YMIN)+0.5
354 MY=43-MY
355 IARG=37
356 IF (0.5.LT.CHAR(I).AND.CHAR(I).LT.36.5) IARG=CHAR(I)+0.5
357 IGRAPH(MY,MX)=IPLOT(IARG)
358 CONTINUE
359
360 470
361 C
362 C
363 C
364
365 DO 480 I=1,45
366 IP2=I+2
367 IFLAG=IP2-(IP2/5)*5
368 K=IP2/5
369 IF (IFLAG.NE.0) WRITE (IPR,490) ( IGRAPH(I,J),J=1,109)
370 IF (IFLAG.EQ.0) WRITE (IPR,500) YLABE(K), ( IGRAPH(I,J),J=1,109)
371 CONTINUE
372 WRITE (IPR,510) XMIN,X25,XMID,X75,XMAX
373 WRITE (IPR,540)
374 C
375 FORMAT (1H,20X,109A1)
376 FORMAT (1H,F20.7,109A1)
377 FORMAT (1H,14X,F20.7,5X,F20.7,5X,F20.7,1X,F20.7)
378 FORMAT (1H1,59X,34HRESIDUALS VS. INDEPENDENT VARIABLE//)
379 FORMAT (1H1,53X,47HSTANDARDIZED RESIDUALS VS. INDEPENDENT VARIABLE//)
380 2//)
381 FORMAT (//55X,44HKNOT LOCATIONS ARE INDICATED BY THE SYMBOL X/)
382 RETURN
383 END

```

```

CPR*NS(1).PLOTSR(1)
1 SUBROUTINE PLOTSR (X,N,NX,HOR,RES,CHAR,NKX,T,K,KX)
2 C-----
3 C PLOTSR WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6 C FOR: PLOTTING KNOT LOCATIONS AND RESIDUALS/STANDARDIZED RESIDUALS
7 C VS. INDEPENDENT VARIABLE
8 C SUBPROGRAMS CALLED: PLOTG
9 C CURRENT VERSION COMPLETED MARCH 14, 1980
10 C-----
11 C DIMENSION X(NX),HOR(NKX),RES(NKX),CHAR(NKX),T(KX)
12 C--- CREATE SUB-VECTORS OF INDEPENDENT VARIABLE AND STANDARDIZED
13 C--- RESIDUALS
14 C DO 10 I=1,N
15 C SWITCH INDEPENDENT VARIABLE AND STANDARD DEVIATIONS OF RESIDUALS
16 C Q=HOR(I)
17 C HOR(I)=X(I)
18 C X(I)=Q
19 C CHAR(I)=10.0
20 C CONTINUE
21 C--- ADD KNOT LOCATIONS TO SUB-VECTORS
22 C DO 20 I=1,K
23 C L=1+N
24 C HOR(L)=T(I)
25 C RES(L)=0.0
26 C CHAR(L)=0.0
27 C CONTINUE
28 C--- GENERATE PLOT OF RESIDUALS VS. INDEPENDENT VARIABLE
29 C NK=N+K
30 C CALL PLOTG (RES,HOR,CHAR,NK,1)
31 C--- CREATE SUB-VECTOR OF STANDARDIZED RESIDUALS
32 C DO 30 I=1,N
33 C IF (X(I).LE.0.0) GO TO 30
34 C RES(I)=RES(I)/X(I)
35 C CONTINUE
36 C--- GENERATE PLOT OF STANDARDIZED RESIDUALS VS. INDEPENDENT VARIABLE
37 C CALL PLOTG (RES,HOR,CHAR,NK,2)
38 C RETURN
39 C END
PLOTSR01
PLOTSR02
PLOTSR03
PLOTSR04
PLOTSR05
PLOTSR06
PLOTSR07
PLOTSR08
PLOTSR09
PLOTSR10
PLOTSR11
PLOTSR12
PLOTSR13
PLOTSR14
PLOTSR15
PLOTSR16
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PLOTSR38
PLOTSR39

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CPR*NS(1).PPREP(2)
1 SUBROUTINE PPREP (T,BCOEF,SCRATCH,BREAK,COEF,KX,JX,NB,MO,IP)
2
3 C PPREP WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6 C FOR: CONVERTING THE B-REPRESENTATION OF THE SPLINE INTO THE
7 C PIECEWISE POLYNOMIAL REPRESENTATION
8 C SUBPROGRAMS CALLED: BSPLPP
9 C CURRENT VERSION COMPLETED APRIL 3, 1980
10
11 C-----
12 DIMENSION T(KX),BCOEF(KX),SCRATCH(JX,JX),BREAK(KX),COEF(JX,KX),
13 2 I1(20)
14
15 10 FORMAT (/1X,50(1H-)/1X,38H* PIECEWISE POLYNOMIAL REPRESENTATION ,
16 2 12HOF SPLINES */1X,50(1H-)//9X,18H....INTERVAL....9X,
17 3 27HCOEFFICIENTS OF (X-X(I))*P//3X,1H1,6X,4HX(I),7X,6HX(I+1),5X,
18 4 3HP = 8(14,8X)/35X,8(14,8X)/35X,4(14,8X)
19
20 20 FORMAT (1X,13,2X,2C12.5,3X,8C12.5/33X,8C12.5/33X,4C12.5)
21
22 30 FORMAT ( )
23
24 40 FORMAT (/1X,42H***** PRINTOUT OF PIECEWISE POLYNOMIALS ,
25 2 18HSUPPRESSED ***** )
26
27 C--- COMPUTE PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINE
28 CALL BSPLPP (T,BCOEF,NB,MO,SCRATCH,BREAK,COEF,L,JX)
29
30 C--- DIVIDE EACH COEF(J,I) BY (J-1) FACTORIAL TO NORMALIZE
31 IF (MO.LT.3) GO TO 80
32 DO 70 I=1,L
33 DO 60 J=3,MO
34 DO 50 K=3,J
35 COEF(J,I)=COEF(J,I)/FLOAT(K-1)
36 CONTINUE
37 CONTINUE
38 IF (IP.EQ.0) GO TO 110
39 DO 90 I=1,MO
40 I1(I)=I-1
41 CONTINUE
42 WRITE (6,10) (I1(I),I=1,MO)
43 WRITE (6,30)
44 DO 100 I=1,L
45 WRITE (6,20) I,BREAK(I),BREAK(I+1),(COEF(J,I),J=1,MO)
46 CONTINUE
47 RETURN
48 WRITE (6,40)
49 RETURN
50 END

```

CPR*NS(1).RESSD(1)

```

1 SUBROUTINE RESSD (X,Y,W,N,NX,NKX,NRSD,T,BCOEF,XXI,K,KX,NB,MO,YHAT,RESSD001
2 RES,RSD,BIATX,JX,IP)
3
4 C-----
5 C RESSD WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
6 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
7 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
8 C FOR: COMPUTING PREDICTED Y-VALUES, STANDARD DEVIATIONS OF
9 C PREDICTED Y-VALUES, AND THE RESIDUAL STANDARD DEVIATION
10 C SUBPROGRAMS CALLED: BVALUE, INTERV, BSPLVB
11 C CURRENT VERSION COMPLETED MARCH 24, 1980
12 C-----
13 DIMENSION X(NX),Y(NX),W(NX),T(NX),BCOEF(KX),YHAT(NKX),RES(NKX),
14 BIATX(JX),XXI(KX,KX)
15
16 10 FORMAT (//1X,25(1H-)/1X,25H* ANALYSIS OF RESIDUALS */1X,25(1H-))//
17 2 9X,6HWEIGHT,20X,8HOBERVED,5X,9HPREDICTED,20X,10HSTD DEV OF/4X,
18 3 1H1,5X,4HW(1),9X,4HX(1),10X,4HY(1),6X,11HRESIDUAL(1),
19 4 3X,14HPREDICTED Y(1)/
20
21 20 FORMAT (1X,14,2X,G11.5,3G14.7,G12.5,G16.7)
22
23 30 FORMAT (//5X,16HRESIDUAL STD DEV,5X,13HRESIDUAL D.F./7X,G12.6,9X,
24 2 15)
25
26 40 FORMAT (/1X,48H***** PRINTOUT OF RESIDUALS SUPPRESSED *****
27 C--- INITIALIZE SUMMING VARIABLE
28 SUM=0.0
29 IF (IP.EQ.0) WRITE (6,40)
30 IF (IP.NE.0) WRITE (6,10)
31
32 C--- COMPUTE PREDICTED VALUES AND RESIDUALS
33 DO 50 I=1,N
34 XX=X(I)
35 YHAT(I)=BVALUE(T,BCOEF,NB,MO,XX,0)
36 RES(I)=Y(I)-YHAT(I)
37 SUM=SUM+W(I)*RES(I)**2
38
39 50 CONTINUE
40
41 C--- COMPUTE RESIDUAL STANDARD DEVIATION
42 RSD=SQRT(SUM/FLOAT(NRSD))
43
44 C--- COMPUTE STANDARD DEVIATIONS OF PREDICTED VALUES
45 DO 90 L=1,N
46 XX=X(L)
47
48 C--- FIND INDEX OF FIRST KNOT TO LEFT OF X-VALUE
49 CALL INTERV (T,K,XX,LEFT,MFLAG)
50
51 C--- CHECK WHETHER X-VALUE LIE WITHIN KNOT SPAN
52 IF (MFLAG.EQ.0) GO TO 60
53
54 C--- SET RESIDUAL TO ZERO FOR X-VALUE OUTSIDE KNOT SPAN
55 RES(L)=0.0
56
57 C--- SET STANDARD DEVIATION OF RESIDUAL TO ZERO
58 YHAT(L)=0.0
59 GO TO 90
60
61 C--- EVALUATE POSSIBLY NON-ZERO B-SPLINES AT X-VALUE
62 CALL BSPLVB (T,MO,1,XX,LEFT,BIATX)
63
64 C--- COMPUTE VARIANCE COEFFICIENT (BIATX)'(XXI)(BIATX) OF
65 PREDICTED Y-VALUE
66 NLOW=LEFT-MO
67 Q1=0.0
68 DO 80 I=1,MO
69 Q2=0.0
70 NI=NLOW+I
71 DO 70 J=1,MO
72 NJ=NLOW+J
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RESSD058
RESSD059
RESSD060
RESSD061
RESSD062
RESSD063
RESSD064
RESSD065
RESSD066
RESSD067
RESSD068
RESSD069
RESSD070
RESSD071
RESSD072

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70 Q2=Q2+BIATX(J)*XXI(NJ,NI)
CONTINUE
80 Q1=Q1+Q2*BIATX(I)
CONTINUE
C--- COMPUTE STANDARD DEVIATION OF PREDICTED Y-VALUE
      YHATSD=RSD*SQRT(Q1)
      IF (IP.EQ.0) GO TO 90
      WRITE (6,20) L,W(L),X(L),Y(L),YHAT(L),RES(L),YHATSD
C--- COMPUTE STANDARD DEVIATION OF EACH RESIDUAL AND STORE IN
C--- VECTOR *YHAT*
      YHAT(L)=SQRT(RSD**2-YHATSD**2)
CONTINUE
90  WRITE (6,30) RSD,NRSD
      RETURN
      END

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CPR*NS(1).RSQ(3)
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SUBROUTINE RSQ (RSD,NRSD,Y,W,N,NX,NNZ)
C-----
C  RSQ  WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
C        DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
C        AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
C        FOR: COMPUTING THE MULTIPLE CORRELATION COEFFICIENT R SQUARE
C        SUBPROGRAMS CALLED: -NONE-
C        CURRENT VERSION COMPLETED JUNE 11, 1980
C-----
C        DIMENSION Y(NX),W(NX)
C        FORMAT (/7X,8HR SQUARE,7X,26HNUMBER OF NON-ZERO WEIGHTS/4X,F11.8,
C        2 16X,15)
C--- COMPUTE RESIDUAL SUM OF SQUARES
C        RSS=FLOAT(NRSD)*RSD**2
C--- INITIALIZE SUMMING VARIABLE
C        TSS=0.0
C        DO 20 I=1,N
C        TSS=TSS+Y(I)*SQRT(W(I))
C        CONTINUE
C--- INITIALIZE SUMMING VARIABLE
C        YN=TSS/FLOAT(NNZ)
C        TSS=0.0
C--- COMPUTE TOTAL SUM OF SQUARES
C        DO 30 I=1,N
C        IF (W(I).EQ.0.0) GO TO 30
C        TSS=TSS+(Y(I)*SQRT(W(I)))-YND**2
C        CONTINUE
C--- COMPUTE R**2
C        R2=1.0-RSS/TSS
C--- TO PRINT OUT R-SQUARED CHANGE THE 'C' IN THE FOLLOWING LINE
C--- TO A BLANK.
C        WRITE (6,10) R2,NNZ
C        RETURN
C        END
RSQ000001
RSQ000002
RSQ000003
RSQ000004
RSQ000005
RSQ000006
RSQ000007
RSQ000008
RSQ000009
RSQ000010
RSQ000011
RSQ000012
RSQ000013
RSQ000014
RSQ000015
RSQ000016
RSQ000017
RSQ000018
RSQ000019
RSQ000020
RSQ000021
RSQ000022
RSQ000023
RSQ000024
RSQ000025
RSQ000026
RSQ000027
RSQ000028
RSQ000029
RSQ000030
RSQ000031
RSQ000032
RSQ000033
RSQ000034

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CPR&NS(1).SDYFIN(1)
1 SUBROUTINE SDYFIN (XF,YFSD,NF,T,K,MO,XXI,KX,RSD,BIATX,JX) SDYFIN01
2 C SDYFIN WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING SDYFIN02
3 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C. SDYFIN03
4 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION SDYFIN04
5 C FOR: COMPUTING THE STANDARD DEVIATION OF THE PREDICTED SDYFIN05
6 C Y-VALUES IN THE FINE MESH SDYFIN06
7 C SUBPROGRAMS CALLED: INTERV, BSPLVB SDYFIN07
8 C CURRENT VERSION COMPLETED OCTOBER 9, 1979 SDYFIN08
9 C SDYFIN09
10 C SDYFIN10
11 C DIMENSION XF(NF),YFSD(NF),T(KX),BIATX(JX),XXI(KX,KX) SDYFIN11
12 C FORMAT (/5X,18H<<<< STD. DEV. OF,15,1X,11HPREDICTED Y,1X, SDYFIN12
13 C 2 21HVALUES COMPUTED >>>>>) SDYFIN13
14 C DO 40 L=1,NF SDYFIN14
15 C XX=XF(L) SDYFIN15
16 C FIND INDEX OF FIRST KNOT TO LEFT OF X-VALUE SDYFIN16
17 C CALL INTERV (T,K,XX,LEFT,MFLAG) SDYFIN17
18 C EVALUATE POSSIBLY NON-ZERO B-SPLINES AT X-VALUE SDYFIN18
19 C CALL BSPLVB (T,MO,1,XX,LEFT,BIATX) SDYFIN19
20 C COMPUTE VARIANCE COEFFICIENT (BIATX)'(XXI)(BIATX) OF SDYFIN20
21 C PREDICTED Y-VALUE SDYFIN21
22 C NLOW=LEFT-MO SDYFIN22
23 C Q1=0.0 SDYFIN23
24 C DO 30 I=1,MO SDYFIN24
25 C Q2=0.0 SDYFIN25
26 C NI=NLOW+I SDYFIN26
27 C DO 20 J=1,MO SDYFIN27
28 C NJ=NLOW+J SDYFIN28
29 C Q2=Q2+BIATX(J)*XXI(NJ,NI) SDYFIN29
30 C CONTINUE SDYFIN30
31 C Q1=Q1+Q2*BIATX(I) SDYFIN31
32 C CONTINUE SDYFIN32
33 C COMPUTE STANDARD DEVIATION OF PREDICTED Y-VALUE SDYFIN33
34 C YFSD(L)=RSD*SQR(Q1) SDYFIN34
35 C CONTINUE SDYFIN35
36 C WRITE (6,10) NF SDYFIN36
37 C RETURN SDYFIN37
38 C END SDYFIN38

```

```

1      SUBROUTINE SORT1 (X,M,N,NX)
2
3      SORT1  OBTAINED BY CHARLES P. REEVE FROM DR. D. A. ZAHN AT
4      THE FLORIDA STATE UNIVERSITY, TALLAHASSEE, FLORIDA
5      UNDER THE NAME *FTASORT*. SEVERAL MINOR CORRECTIONS
6      WERE MADE TO THE ORIGINAL VERSION AFTER LINE 61.
7      FOR: SORTING THE SEGMENT OF A REAL ARRAY BETWEEN ENTRIES
8      M AND N FROM SMALLEST TO LARGEST
9      SUBROUTINES CALLED: -NONE-
10     CURRENT VERSION COMPLETED JANUARY 30, 1978
11     NOTE: ARRAYS LP(K) AND LQ(K) PERMIT SORTING UP TO 2*(K+1)-1
12           ELEMENTS, I.E., FOR K=25 YOU MAY SORT 67,108,863 ELEMENTS.
13
14     DIMENSION LP(25),LQ(25),X(NX)
15     I=1
16     KN=M
17     KN=N
18     IF (KM.GE.KN) GO TO 70
19     J=KM
20     K=(KN+KN)/2
21     A=X(K)
22     IF (X(KN).LE.A) GO TO 20
23     X(K)=X(KN)
24     X(KN)=A
25     A=X(K)
26     L=KN
27     IF (X(KN).GE.A) GO TO 40
28     X(K)=X(KN)
29     X(KN)=A
30     A=X(K)
31     IF (X(KN).LE.A) GO TO 40
32     X(K)=X(KN)
33     X(KN)=A
34     A=X(K)
35     GO TO 40
36     X(L)=X(J)
37     X(J)=B
38     L=L-1
39     IF (X(L).GT.A) GO TO 40
40     B=X(L)
41     J=J+1
42     IF (X(J).LT.A) GO TO 50
43     IF (J.LE.L) GO TO 36
44     IF (L-KM.LE.KN-J) GO TO 60
45     LP(I)=KM
46     LQ(I)=L
47     KN=J
48     I=I+1
49     GO TO 80
50     LP(I)=J
51     LQ(I)=KN
52     KN=L
53     I=I+1
54     GO TO 80
55     I=I-1
56     IF (I.EQ.0) RETURN
57     KI=LP(I)

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SORT1001
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 SORT1003
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58 KN=LQ(I)
 59 IF (KN-KM.GE.11) GO TO 10
 60 KM=KM-1
 61 KM=KM+1
 62 IF (KM.EQ.KN) GO TO 70
 63 A=X(KM+1)
 64 IF (X(KM).LE.A) GO TO 90
 65 J=KM
 66 X(J+1)=X(J)
 67 J=J-1
 68 IF (J.EQ.M-1) GO TO 110
 69 IF (A.LT.X(J)) GO TO 100
 70 X(J+1)=A
 71 GO TO 90
 72 END

```

1 SUBROUTINE SORT2 (X,Y,M,N,NX)
2
3 SORT2  OBTAINED BY CHARLES P. REEVE FROM DR. D. A. ZAHN AT
4 THE FLORIDA STATE UNIVERSITY, TALLAHASSEE, FLORIDA
5 UNDER THE NAME *FTASORT*. SEVERAL MINOR CORRECTIONS
6 WERE MADE TO THE ORIGINAL VERSION AFTER LINE 61.
7 THE PROGRAM HAS BEEN ALTERED SO THAT A SECOND ARRAY IS
8 CARRIED ALONG AND SORTED IDENTICALLY AS THE FIRST
9 FOR: SORTING THE SEGMENT OF A REAL ARRAY BETWEEN ENTRIES
10 M AND N FROM SMALLEST TO LARGEST
11 SUBROUTINES CALLED: -NONE-
12 CURRENT VERSION COMPLETED MARCH 24, 1980
13 NOTE: ARRAYS LP(K) AND LQ(K) PERMIT SORTING UP TO 2*(K+1)-1
14 ELEMENTS, I.E., FOR K=25 YOU MAY SORT 67,108,863 ELEMENTS.
15
16 DIMENSION LP(25),LQ(25),X(NX),Y(NX)
17 I=1
18 KN=M
19 KN=N
20 IF (KM.GE.KN) GO TO 70
21 J=KM
22 K=(KN+KM)/2
23 A=X(K)
24 B=Y(K)
25 IF (X(KM).LE.A) GO TO 20
26 X(K)=X(KM)
27 Y(K)=Y(KM)
28 X(KM)=A
29 Y(KM)=B
30 A=X(K)
31 B=Y(K)
32 L=KN
33 IF (X(KN).GE.A) GO TO 40
34 X(K)=X(KN)
35 Y(K)=Y(KN)
36 X(KN)=A
37 Y(KN)=B
38 A=X(K)
39 B=Y(K)
40 IF (X(KM).LE.A) GO TO 40
41 X(K)=X(KM)
42 Y(K)=Y(KM)
43 X(KM)=A
44 Y(KM)=B
45 A=X(K)
46 B=Y(K)
47 GO TO 40
48 X(L)=X(J)
49 Y(L)=Y(J)
50 X(J)=C
51 Y(J)=H
52 L=L-1
53 IF (X(L).GT.A) GO TO 40
54 C=X(L)
55 H=Y(L)
56 J=J+1
57 IF (X(J).LT.A) GO TO 50

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SORT2001
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 SORT2090

IF (J.LE.L) GO TO 30
 IF (L-KM.LE.KN-J) GO TO 60
 LP(I)=KM
 LQ(I)=L
 KM=J
 I=I+1
 GO TO 80
 LP(I)=J
 LQ(I)=KN
 KN=L
 I=I+1
 GO TO 80
 I=I-1
 IF (I.EQ.0) RETURN
 KM=LP(I)
 KN=LQ(I)
 IF (KN-KM.GE.11) GO TO 10
 KM=KM-1
 KM=KM+1
 IF (KM.EQ.KN) GO TO 70
 A=X(KM+1)
 B=Y(KM+1)
 IF (X(KM).LE.A) GO TO 90
 J=KM
 X(J+1)=X(J)
 Y(J+1)=Y(J)
 J=J-1
 IF (J.EQ.M-1) GO TO 110
 IF (A.LT.X(J)) GO TO 100
 X(J+1)=A
 Y(J+1)=B
 GO TO 90
 END

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1 SUBROUTINE SPLLEN (H,X,Y,W,R1,R2,RES,N,NX,NKX,T,BCOEF,XXI,Q,DIAG,KSPLEE001
 2 2.KX,YY,NY,NYX,MD,SCRATCH,JX,AL,DL,C,IP)
 3

4 SPLLEN WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
 5 DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
 6

7 * * * * *
 8 * FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION *
 9 * * * * *

10 THIS PACKAGE OF SUBROUTINES WAS WRITTEN FOR THE FOLLOWING
 11 CALIBRATION PROCEDURES:
 12

13 1) A MONOTONIC SEQUENCE OF RESPONSES $Y(1)$, $Y(2)$, ..., $Y(N)$
 14 EACH CONTAINING SOME ERROR ARE OBSERVED AT KNOWN POINTS
 15 $X(1)$, $X(2)$, ..., $X(N)$ WHERE $X(1) < X(2) < \dots < X(N)$.
 16

17 2) A SPLINE OF SPECIFIED DEGREE WITH A SPECIFIED SEQUENCE OF
 18 FIXED KNOTS IS FIT TO THE Y-VALUES WHICH MAY BE WEIGHTED.
 19

20 3) THE RESIDUAL STANDARD DEVIATION IS COMPUTED IN ORDER TO
 21 MEASURE THE GOODNESS OF THE SPLINE FIT.
 22

23 4) PREDICTED RESPONSE VALUES ARE COMPUTED AT A LARGE NUMBER
 24 OF UNIFORMLY SPACED X-VALUES BETWEEN THE EXTREME KNOTS.
 25 A CONFIDENCE INTERVAL FOR EACH PREDICTED RESPONSE IS
 26 COMPUTED BASED ON SPECIFIED CONSTANTS ALPHA, BETA, AND C
 27 IN ACCORDANCE WITH REFERENCE PAPER BY SCHEFFE GIVEN BELOW.
 28

29 5) FOR SPECIFIED Y-VALUES, INVERSE INTERPOLATION IS APPLIED
 30 TO THE CALIBRATION CURVE AND ITS CONFIDENCE BAND TO GIVE
 31 PREDICTED X-VALUES WITH CORRESPONDING UPPER AND LOWER
 32 CONFIDENCE LIMITS.
 33

34 PASSED PARAMETERS (AND DIMENSIONS):
 35

36 * H(80) = UP TO 80 CHARACTERS IN 80A1 FORMAT IDENTIFYING THE
 37 DATA
 38

39 * X(NX) = VECTOR (LENGTH N) OF X-VALUES WHERE OBSERVATIONS
 40 WERE MADE (INDEPENDENT VARIABLE)
 41

42 * Y(NX) = VECTOR (LENGTH N) OF OBSERVATIONS
 43

44 * W(NX) = VECTOR (LENGTH N) OF WEIGHTS FOR OBSERVATIONS
 45

46 R1(NKX) = VECTOR (LENGTH N+K) FOR SCRATCH AREA
 47

48 R2(NKX) = VECTOR (LENGTH N+K) FOR SCRATCH AREA
 49

50 RES(NKX) = VECTOR (LENGTH N+K) OF RESIDUALS FROM SPLINE FIT
 51

52 * N = NUMBER OF OBSERVATIONS
 53

54 * NX = DIMENSION (>=N) OF VECTORS X,Y,W
 55

56 * NKX = DIMENSION (>=N+K) OF VECTORS R1,R2,RES
 57

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 KSPLEE057

58 C * T(KX) = VECTOR (LENGTH K+2*MD) OF KNOT LOCATIONS

59 C BCOEF(KX) = VECTOR (LENGTH K+MD-1) OF B-SPLINE COEFFICIENTS

60 C XXI(KX,KX) = VARIANCE-COVARIANCE MATRIX (SIZE [K+MD-1]X[K+MD-1])

61 C OF B-SPLINE COEFFICIENTS

62 C Q(JX,KX) = MATRIX (SIZE [MD+1]X[K+MD-1]) FOR SCRATCH AREA

63 C DIAG(KX) = VECTOR (LENGTH K+MD-1) FOR SCRATCH AREA

64 C * K = NUMBER OF KNOTS SPECIFIED BY USER (LATER INCREASED

65 C TO K+2*MD BY PROGRAM)

66 C * KX = DIMENSION (>=K+2*MD) OF VECTORS T, BCOEF, DIAG AND

67 C MATRICES XXI AND Q (COLUMN ONLY)

68 C * YY(NYX) = VECTOR (LENGTH NY) OF Y-VALUES FOR WHICH PREDICTED

69 C X-VALUES (WITH CONFIDENCE INTERVALS) ARE TO BE

70 C COMPUTED

71 C * NY = NUMBER OF Y-VALUES FOR WHICH PREDICTED X-VALUES

72 C ARE TO BE COMPUTED

73 C * NYX = DIMENSION (>=NY) OF VECTOR YY

74 C * MD = DEGREE OF SPLINE (<=19); FOR EXAMPLE, 1=LINEAR,

75 C 2=QUADRATIC, 3=CUBIC

76 C * SCRTCH(JX,JX) = MATRIX (SIZE [MD+1]X[MD+1]) FOR SCRATCH AREA

77 C * JX = DIMENSION OF SQUARE MATRIX SCRATCH AND ROW

78 C DIMENSION OF MATRIX Q = 20

79 C * AL = ALPHA LEVEL OF SIGNIFICANCE (SEE REFERENCE BELOW)

80 C * DL = DELTA LEVEL OF SIGNIFICANCE (SEE REFERENCE BELOW)

81 C * C = CONSTANT IN THE INTERVAL (0.85,1.25) ASSOCIATED

82 C WITH SCHEFFE'S CALIBRATION TECHNIQUE

83 C 0 FOR ABBREVIATED PRINTOUT (NO RESIDUALS)

84 C * IP = 1 FOR FULL PRINTOUT (RESIDUALS, PP REPRESENTATION)

85 C 2 FOR FULL PRINTOUT PLUS Y-CONFIDENCE INTERVALS FOR

86 C 300 EVENLY SPACED X-VALUES OVER KNOT SPAN

87 C * INDICATES THAT AN INPUT VALUE IS REQUIRED FOR THIS VARIABLE

88 C NOTE: THE USER IS NOT REQUIRED TO ORDER THE ELEMENTS OF ANY INPUT

89 C VECTOR. THE PROGRAM WILL AUTOMATICALLY ORDER THOSE VECTORS

90 C WHICH NEED TO BE ORDERED.

91 C REFERENCE: SCHEFFE, HENRY, 'A STATISTICAL THEORY OF CALIBRATION',

92 C THE ANNALS OF STATISTICS, VOLUME 1, NUMBER 1,

93 C JANUARY 1973, PP. 1-37

94 C SUBPROGRAMS CALLED: ADKNTS, CHECK1, CHECK2, CIFYIN, COVAR, L2APPR,

SPLEE058

SPLEE059

SPLEE060

SPLEE061

SPLEE062

SPLEE063

SPLEE064

SPLEE065

SPLEE066

SPLEE067

SPLEE068

SPLEE069

SPLEE070

SPLEE071

SPLEE072

SPLEE073

SPLEE074

SPLEE075

SPLEE076

SPLEE077

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PLOTSR, PPREP, RESSD, RSQ, SDYFIN, SORT1,
SORT2, XYFINE, YTOXCI
CURRENT VERSION COMPLETED JUNE 11, 1980

SET DIMENSIONS OF VECTORS AND MATRIX
DIMENSION X(NX), Y(NX), W(NX), R1(NKX), R2(NKX), RES(NKX)
DIMENSION T(KX), Q(JX, KX), DIAG(KX), BCOEF(KX), XXI(KX, KX)
DIMENSION YY(NYX), SCRTCH(JX, JX), BIATX(20), H(80)
PARAMETER NF=300
DIMENSION XF(300), YF(300), YFL(300), YFU(300), YFSD(300)
FORMAT (1H/1X, 45(1H*/1X, 32H* FIXED-KNOT SPLINE PACKAGE FOR ,
2 13HCALIBRATION */1X, 45(1H*))
FORMAT (//1X, 39(1H-)/1X, 25H* ESTIMATION OF B-SPLINE ,
2 14HCOEFFICIENTS */1X, 39(1H-))
FORMAT (/9X, 8HB-SPLINE/4X, 1H1, 5X, 4HCOEF, 10X, 7HSTD DEV/)
FORMAT (1X, 14, 2C15.8)
FORMAT (/1X, 42H***** PRINTOUT OF B-SPLINE COEFFICIENTS ,
2 18HSUPPRESSED *****)
FORMAT (//1X, 42(1H-)/1X, 37H* PARAMETERS OF LEAST SQUARES SPLINE ,
2 5HFIT */1X, 42(1H-)/13X, 18HDEGREE OF SPLINE =, 14/3X,
3 28HNUMBER OF OBSERVATIONS =, 14/3X,
4 28HNUMBER OF ZERO WEIGHTS =, 14/3X, 19HNUMBER OF NON-ZERO ,
5 9HWEIGHTS =, 14/3X, 28HNUMBER OF KNOTS =, 14/3X,
6 28HNUMBER OF B-SPLINES =, 14/11X, 18HNUMBER OF Y-VALUES/7X
7, 24HFOR WHICH X CONFIDENCE =, 14/3X, 18HINTERVAL IS TO BE ,
8 8HCOMPUTED)
FORMAT (//5X, 25H----- FULL PRINTOUT -----/)
FORMAT (//5X, 32H----- ABBREVIATED PRINTOUT -----/)
FORMAT (//1X, 80A1)
FORMAT (//1X, 8(1H*/1X, 8H* STOP */1X, 8(1H*/))
NF=300
DEFINE NUMBER OF POINTS IN FINE MESH

WRITE HEADING FOR HARDCOPY OUTPUT
WRITE (6, 10)
WRITE RUN IDENTIFICATION
WRITE (6, 90) (H(1), I=1, 80)
IF (IP.GE.1) WRITE (6, 70)
IF (IP.EQ.0) WRITE (6, 80)
COMPUTE ORDER OF SPLINE
MO=MD+1
CHECK THAT INPUT PARAMETERS FALL WITHIN ALLOWABLE RANGES

CALL CHECK1 (W, N, NX, K, KX, NKX, NY, NYX, JX, MO, AL, DL, C, NZ)
SORT THE VECTOR OF KNOT LOCATIONS FROM LEAST TO GREATEST

CALL SORT1 (T, 1, K, KX)

SORT THE VECTOR OF X-VALUES FROM LEAST TO GREATEST AND CARRY
ALONG THE CORRESPONDING Y-VALUES

CALL SORT2 (X, Y, 1, N, NX)

CHECK FOR OBSERVATIONS OUTSIDE KNOT SEQUENCE

CALL CHECK2 (T, K, KX, X, W, N, NX, NZ, MO)

COMPUTE NUMBER OF NON-ZERO WEIGHTS

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174	NNZ=N-NZ	SPLEE174
175	C--- DEFINE NEW VECTOR OF KNOTS WITH END POINTS DUPLICATED	SPLEE175
176	C--- (MD) TIMES	SPLEE176
177	C	SPLEE177
178	CALL ADKNTS (T,K,KX,MO)	SPLEE178
179	C	SPLEE179
180	C--- COMPUTE NUMBER OF B-SPLINES	SPLEE180
181	NB=K-MO	SPLEE181
182	C--- COMPUTE NUMBER OF DEGREES OF FREEDOM FOR RESIDUALS	SPLEE182
183	NRSD=NNZ-NB	SPLEE183
184	WRITE (6,60) MD,N,NZ,NNZ,K,NB,NY	SPLEE184
185	C--- COMPUTE ESTIMATES OF B-SPLINE COEFFICIENTS	SPLEE185
186	C	SPLEE186
187	CALL L2APPR (T,NB,MO,Q,DIAG,BCOEF,JX,K,N,X,Y,W)	SPLEE187
188	C	SPLEE188
189	C--- COMPUTE UNSCALED VARIANCE-COVARIANCE MATRIX OF	SPLEE189
190	B-SPLINE COEFFICIENTS	SPLEE190
191	C	SPLEE191
192	CALL COVAR (KX,NB,JX,MO,Q,XXI)	SPLEE192
193	C	SPLEE193
194	C--- COMPUTE (PREDICTED Y-VALUES AND) RESIDUAL STANDARD DEVIATION	SPLEE194
195	C	SPLEE195
196	CALL RESSD (X,Y,W,N,NX,NKX,NRSD,T,BCOEF,XXI,K,KX,NB,MO,R1,RES,RSD,	SPLEE196
197	2BIATX,JX,IP)	SPLEE197
198	C	SPLEE198
199	IF (IP.EQ.0) WRITE (6,50)	SPLEE199
200	IF (IP.EQ.0) GO TO 120	SPLEE200
201	C--- WRITE B-SPLINE COEFFICIENTS AND THEIR STANDARD DEVIATIONS	SPLEE201
202	WRITE (6,20)	SPLEE202
203	DO 110 I=1,NB	SPLEE203
204	WRITE (6,30)	SPLEE204
205	S=RSD*SQRT(XXI(I,I))	SPLEE205
206	WRITE (6,40) I,BCOEF(I),S	SPLEE206
207	CONTINUE	SPLEE207
208	C--- COMPUTE MULTIPLE CORRELATION COEFFICIENT R-SQUARED (THIS VALUE IS	SPLEE208
209	NOT PRINTED. TO PRINT R-SQUARED MAKE A CHANGE IN SUBROUTINE RSQ.)	SPLEE209
210	C	SPLEE210
211	120 CALL RSQ (RSD,NRSD,Y,W,N,NX,NNZ)	SPLEE211
212	C	SPLEE212
213	C--- CREATE FINE MESH OF EVENLY SPACED X-VALUES BETWEEN END KNOTS	SPLEE213
214	C--- AND COMPUTE PREDICTED Y-VALUES THERE	SPLEE214
215	C	SPLEE215
216	CALL XYFINE (NF,T,BCOEF,K,KX,NB,MO,XF,YF)	SPLEE216
217	C	SPLEE217
218	C--- COMPUTE STANDARD DEVIATION OF PREDICTED Y-VALUES	SPLEE218
219	C	SPLEE219
220	CALL SDYFIN (XF,YFSD,NF,T,K,MO,XXI,KX,RSD,BIATX,JX)	SPLEE220
221	C	SPLEE221
222	C--- COMPUTE CONFIDENCE INTERVALS FOR PREDICTED Y-VALUES USING	SPLEE222
223	C--- SCHEFFE'S TECHNIQUE (SEE REFERENCE IN SUBROUTINE CIYFIN)	SPLEE223
224	C	SPLEE224
225	CALL CIYFIN (XF,YF,YFSD,NF,RSD,AL,DL,C,NRSD,NB,YFL,YFU,IP)	SPLEE225
226	C	SPLEE226
227	C--- COMPUTE X CONFIDENCE INTERVALS FOR SPECIFIED Y-VALUES	SPLEE227
228	C	SPLEE228
229	CALL YTOXCI (XF,YFL,YF,YFU,NF,YY,NY,NYX)	SPLEE229
230	C	SPLEE230
231	C--- COMPUTE PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINE	SPLEE231

SPLEE232
SPLEE233
SPLEE234
SPLEE235
SPLEE236
SPLEE237
SPLEE238
SPLEE239
SPLEE240
SPLEE241

C CALL PPREP (T,BCOEF,SCRATCH,DIAC,Q,KX,JX,NB,MO,IP)
C
C--- PLOT KNOT LOCATIONS AND RESIDUALS VS. INDEPENDENT VARIABLE
C
C CALL PLOTSR (X,N,NX,R1,RES,R2,NKX,T,K,KX)
C
C WRITE (6,100)
C RETURN
C END

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CPR*NS(1).XYFINE(1)
1 SUBROUTINE XYFINE (NF,T,BCOEF,K,KX,NB,MO,XF,YF)
2
3 C XYFINE WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
4 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
5 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
6 C FOR: CREATING A FINE MESH OF VALUES OVER THE DOMAIN OF X-VALUES
7 C WHERE OBSERVATIONS WERE MADE AND COMPUTING CORRESPONDING
8 C PREDICTED Y-VALUES
9 C SUBPROGRAMS CALLED: BVALUE
10 C CURRENT VERSION COMPLETED MARCH 19, 1980
11
12 C-----
13 C DIMENSION T(KX),BCOEF(KX),XF(NF),YF(NF)
14 C--- CREATE FINE MESH OF X VALUES OVER INTERVAL SPANNED BY KNOTS
15 10 FORMAT (//5X,13H<<<<< GRID OF,15,1X,24H EVENLY SPACED X VALUES ,
16 2 13HCREATED >>>>>)
17 C=(T(K)-T(1))/FLOAT(NF-1)
18 DO 20 I=1,NF
19 XF(I)=FLOAT(I-1)*C+T(1)
20 C CONTINUE
21 C--- COMPUTE PREDICTED Y VALUE AT EACH X VALUE
22 DO 30 I=1,NF
23 XX=XF(I)
24 YF(I)=BVALUE(T,BCOEF,NB,MO,XX,0)
25 C CONTINUE
26 WRITE (6,10) NF
27 RETURN
END
XYFINE01
XYFINE02
XYFINE03
XYFINE04
XYFINE05
XYFINE06
XYFINE07
XYFINE08
XYFINE09
XYFINE10
XYFINE11
XYFINE12
XYFINE13
XYFINE14
XYFINE15
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XYFINE20
XYFINE21
XYFINE22
XYFINE23
XYFINE24
XYFINE25
XYFINE26
XYFINE27

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1 SUBROUTINE YTOXC1 (XF, YFL, YF, YFU, NF, YY, NY, NYX)
2
3 C-----
4 C YTOXC1 WRITTEN BY CHARLES P. REEVE, STATISTICAL ENGINEERING
5 C DIVISION, NATIONAL BUREAU OF STANDARDS, WASHINGTON, D.C.
6 C AS PART OF THE FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION
7 C FOR: COMPUTING X CONFIDENCE INTERVALS FOR GIVEN Y-VALUES BY
8 C INVERSE INTERPOLATION ON THE CALIBRATION CURVE AND ITS
9 C UPPER AND LOWER BOUNDS
10 C SUBPROGRAMS CALLED: GETX, SORT1
11 C CURRENT VERSION COMPLETED SEPTEMBER 3, 1980
12 C-----
13 C DIMENSION XF(NF), YFL(NF), YF(NF), YFU(NF), YY(NYX), IND(6)
14 C 2 IH<, 1H<
15
16 10 FORMAT (/5X, 40H<<<< NO Y-VALUES SPECIFIED FOR INVERSE ,
17 2 19HINTERPOLATION >>>>)
18
19 20 FORMAT (/1X, 47H*** LOWER CONFIDENCE CURVE IS NOT MONOTONIC AT ,
20 2 4HYFL(, 14, 3H) =, G12.7/5X, 21HNO INTERPOLATION DONE)
21
22 30 FORMAT (/1X, 45H*** CALIBRATION CURVE IS NOT MONOTONIC AT YF(, 14,
23 2 3H) =, G12.7/5X, 21HNO INTERPOLATION DONE)
24
25 40 FORMAT (/1X, 47H*** UPPER CONFIDENCE CURVE IS NOT MONOTONIC AT ,
26 2 4HYFU(, 14, 3H) =, G12.7/5X, 21HNO INTERPOLATION DONE)
27
28 50 FORMAT (/1X, 65(1H-)/1X, 29H* COMPUTATION OF CALIBRATION ,
29 2 36HINTERVALS BY INVERSE INTERPOLATION */1X, 65(1H-)/24X,
30 3 11HLOWER LIMIT, 7X, 9HPREDICTED, 7X, 11HUPPER LIMIT/4X, 1H1, 6X, 4HY(1),
31 4 12X, 5HFOR X, 14X, 1HX, 14X, 5HFOR X/)
32
33 60 FORMAT (1X, 14, G15.7, 3(3X, A1, G13.7))
34
35 70 FORMAT (/1X, 46H*** AT LEAST ONE Y-VALUE IS OUTSIDE THE RANGE ,
36 2 3H***1X, 49H*** OF AT LEAST ONE CALIBRATION CURVE ***/)
37
38 80 FORMAT (/5X, 40HS DENOTES THE VALUE OF THE SMALLEST KNOT
39 90 2 4HYFL(, 14, 3H) DENOTES THE VALUE OF THE LARGEST KNOT)
40
41 100 FORMAT (/5X, 41H* DENOTES VALUES OUTSIDE THE RANGE OF THE,
42 2 22H CALIBRATION DATA - NO/7X, 29HVALID PREDICTION IS AVAILABLE)
43
44 110 FORMAT (/5X, 49H< INDICATES THAT NO VALID LOWER CALIBRATION LIMIT/
45 2 7X, 55HGREATER THAN THE MINIMUM POSSIBLE X-VALUE IS AVAILABLE.)
46
47 120 FORMAT (/5X, 49H> INDICATES THAT NO VALID UPPER CALIBRATION LIMIT/
48 2 7X, 55HSMALLER THAN THE MAXIMUM POSSIBLE X-VALUE IS AVAILABLE.)
49
50 WRITE (6, 50)
51 IF (NY.LT.1) GO TO 230
52 M=1
53 IF (YF(1).GT.YF(NF)) M=-1
54 NF1=NF-1
55
56 C--- CHECK WHETHER CALIBRATION CURVE AND BOUNDS ARE MONOTONIC
57 DO 150 J=1, NF1
58 D=(YFL(J+1)-YFL(J))*FLOAT(M)
59 IF (D.GT.0.0) GO TO 130
60 J1=J+1
61 WRITE (6, 20) J1, YFL(J1)
62 RETURN
63 D=(YF(J+1)-YF(J))*FLOAT(M)
64 IF (D.GT.0.0) GO TO 140
65 J1=J+1
66 WRITE (6, 30) J1, YF(J1)
67 RETURN
68 D=(YFU(J+1)-YFU(J))*FLOAT(M)
69 IF (D.GT.0.0) GO TO 150
70 J1=J+1

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58 WRITE (6,40) J1,YFU(J1)
59 RETURN
60 CONTINUE
61 C--- ORDER VECTOR OF Y-VALUES FOR WHICH X CONFIDENCE LIMITS ARE TO
62 C--- BE COMPUTED
63 CALL SORT1 (YY,1,NY,NYX)
64 L1=0
65 L2=0
66 L3=0
67 KS=0
68 KL=0
69 C--- IF CURVE IS MONOTONE DECREASING INVERT VECTORS ASSOCIATED
70 C--- WITH FINE MESH OF POINTS
71 IF (M.EQ.1) GO TO 170
72 NHALF=NF/2
73 DO 160 I=1,NHALF
74 J=NF+1-I
75 Q=XF(I)
76 XF(I)=XF(J)
77 XF(J)=Q
78 Q=YFL(I)
79 YFL(I)=YFL(J)
80 YFL(J)=Q
81 Q=YF(I)
82 YF(I)=YF(J)
83 YF(J)=Q
84 Q=YFU(I)
85 YFU(I)=YFU(J)
86 YFU(J)=Q
87 CONTINUE
88 DO 220 J=1,NY
89 Y=YY(J)
90 C--- GET THREE (3) X-VALUES BY INVERSE INTERPOLATION
91 CALL GETX (XF,YFL,NF,Y,L1,M,XU,I3,KS,KL)
92 IF (I3.EQ.1) GO TO 180
93 I3=(3-15*M+2*I3+6*M*I3)/2
94 CALL GETX (XF,YF,NF,Y,L2,M,X,I2,KS,KL)
95 IF (I2.EQ.1) GO TO 190
96 I2=4
97 X=0.
98 CALL GETX (XF,YFU,NF,Y,L3,M,XL,I1,KS,KL)
99 IF (I1.EQ.1) GO TO 200
100 I1=(3+15*M+2*I1-6*M*I1)/2
101 C--- IF CURVE IS MONOTONE DECREASING REVERSE LIMITS
102 IF (M.EQ.1) GO TO 210
103 D=XL
104 XL=XU
105 XU=D
106 I=I1
107 I1=I3
108 I3=I
109 WRITE (6,60) J,Y,IND(I1),XL,IND(I2),X,IND(I3),XU
110 CONTINUE
111 C--- FLAG Y-VALUES WHICH GIVE INTERPOLATED X-VALUES OUTSIDE THE KNOT
112 C--- SPAN
113 IF (KS+KL.EQ.0) RETURN
114 WRITE (6,70)
115 WRITE (6,80)

```

YTOXC058
 YTOXC059
 YTOXC060
 YTOXC061
 YTOXC062
 YTOXC063
 YTOXC064
 YTOXC065
 YTOXC066
 YTOXC067
 YTOXC068
 YTOXC069
 YTOXC070
 YTOXC071
 YTOXC072
 YTOXC073
 YTOXC074
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 YTOXC105
 YTOXC106
 YTOXC107
 YTOXC108
 YTOXC109
 YTOXC110
 YTOXC111
 YTOXC112
 YTOXC113
 YTOXC114
 YTOXC115

116
117
118
119
120
121
122
123

WRITE (6,90)
WRITE (6,100)
WRITE (6,110)
WRITE (6,120)
RETURN
WRITE (6,10)
RETURN
END

230

YT0XC116
YT0XC117
YT0XC118
YT0XC119
YT0XC120
YT0XC121
YT0XC122
YT0XC123

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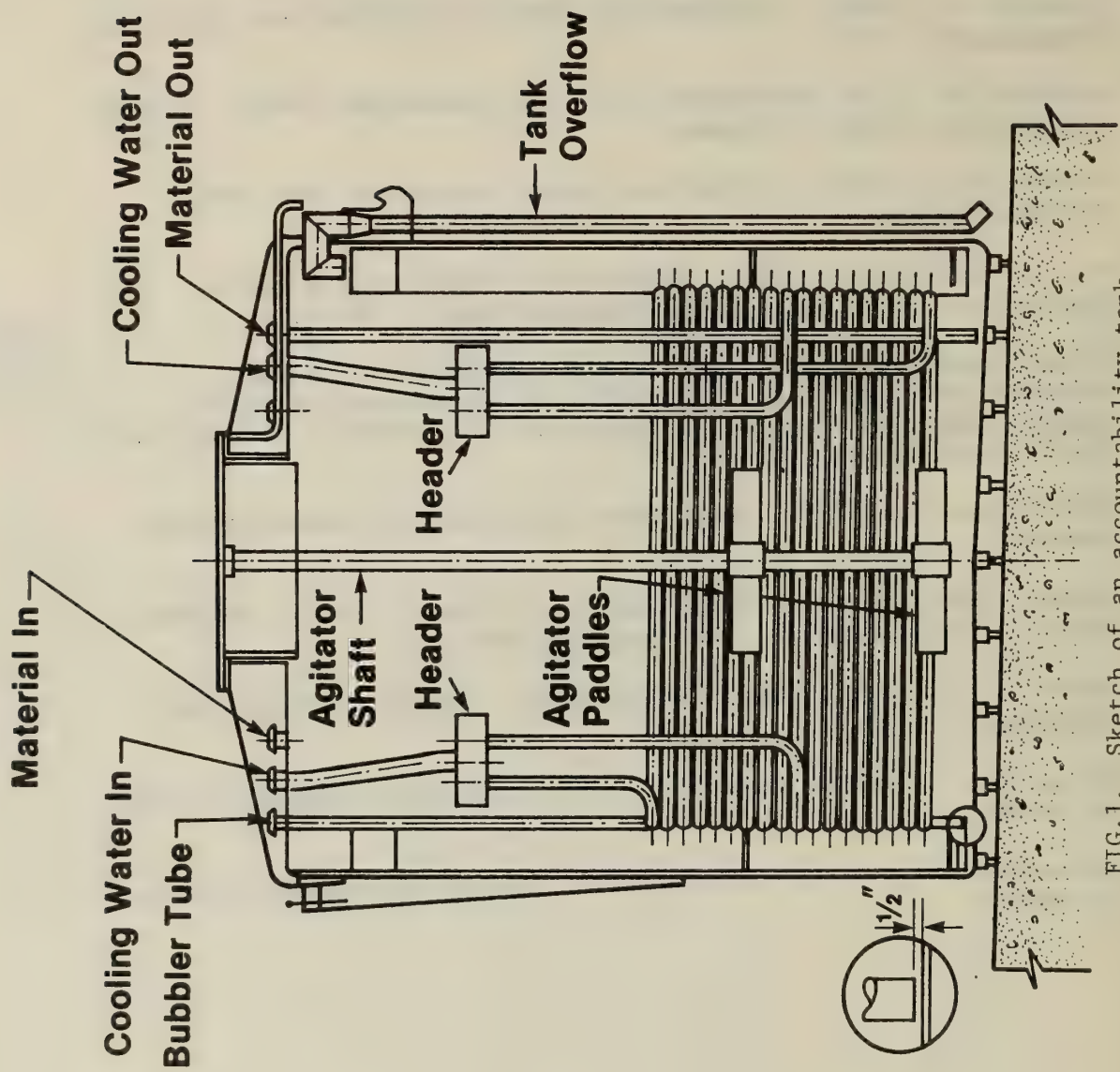


FIG.1. Sketch of an accountability tank.

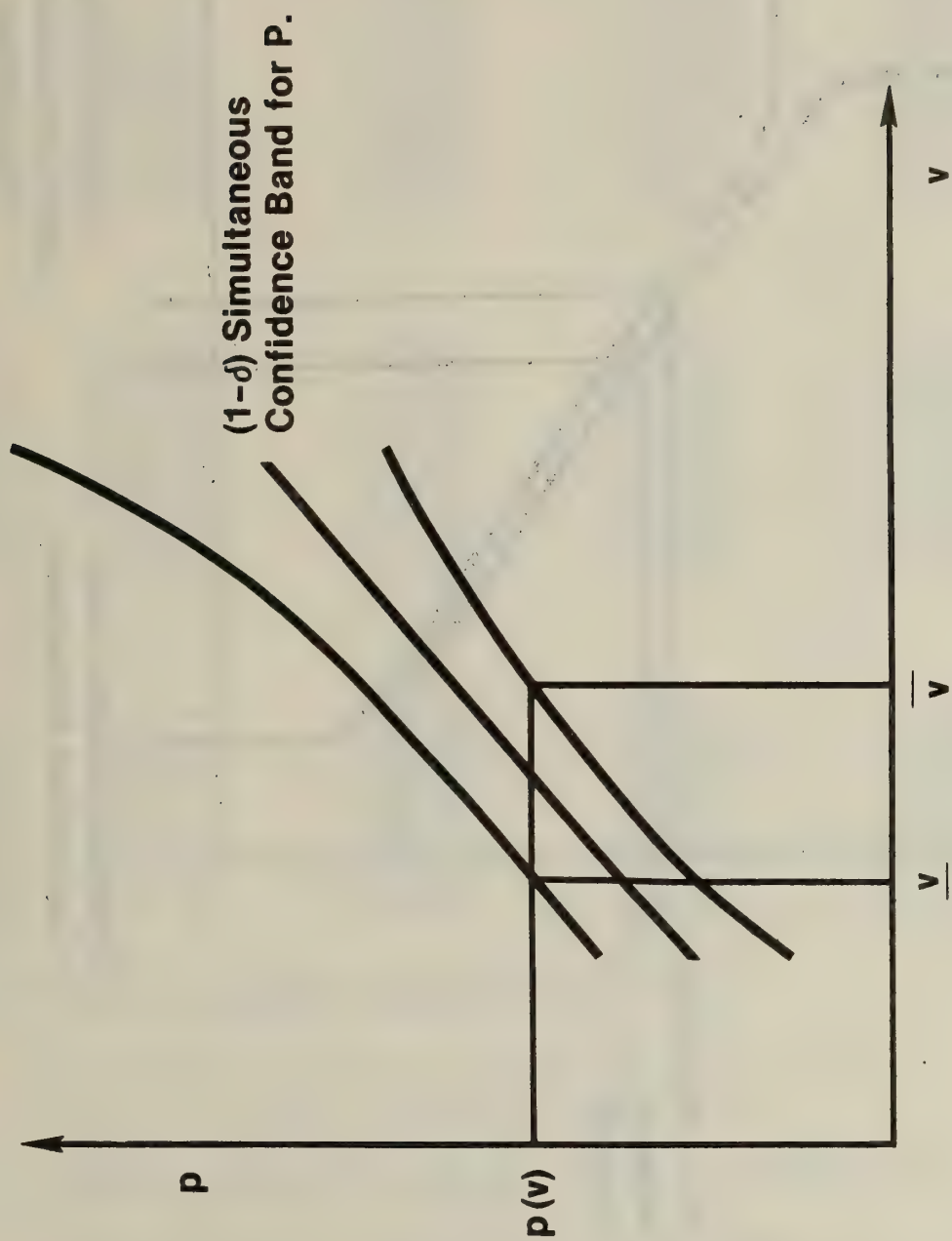


FIG. 2. Hypothetical Interval for v obtained from an exact value of $p = p(v)$.

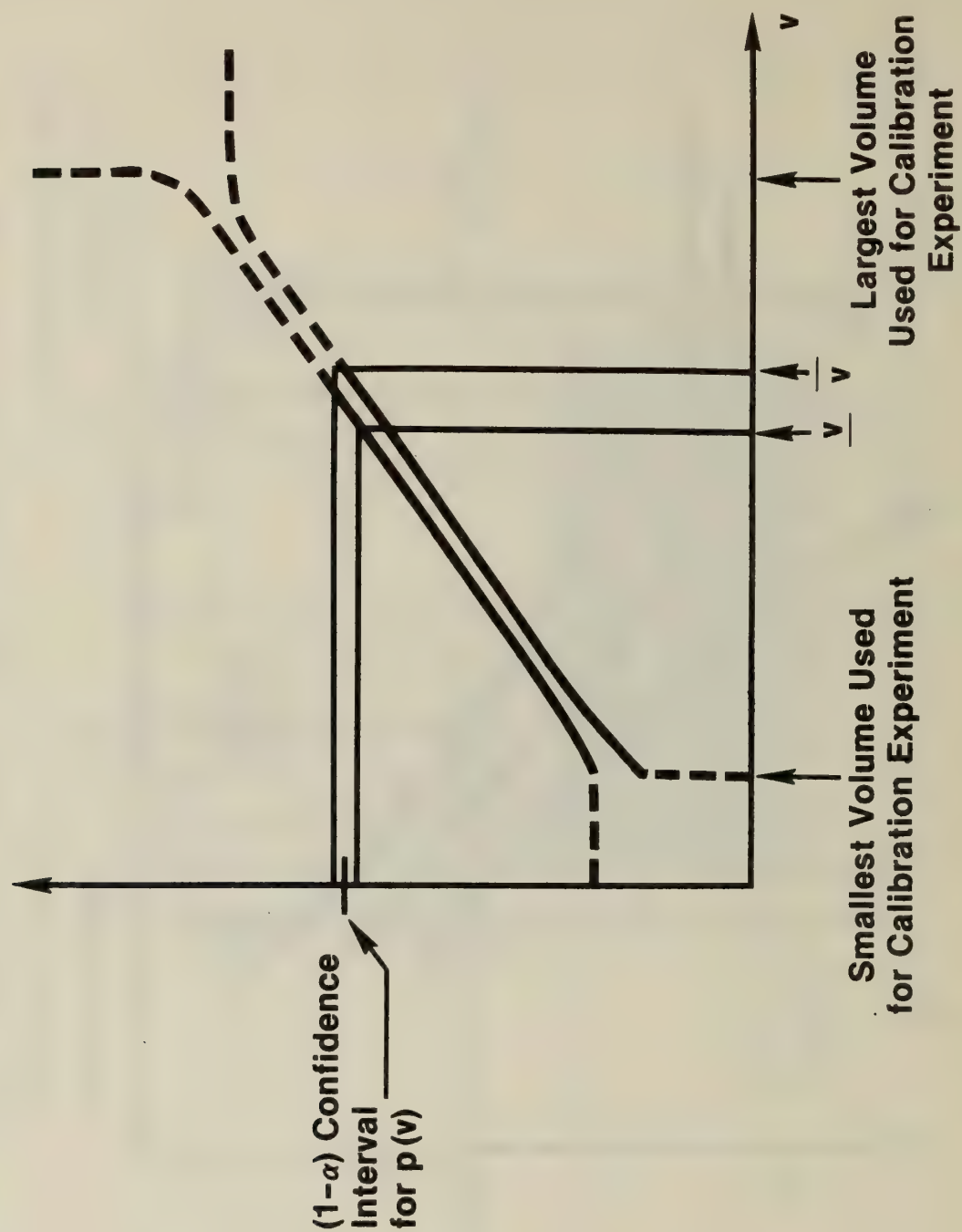


FIG.3. Schematic for approximate construction of the calibration intervals.

* COMPUTATION OF CALIBRATION INTERVALS BY INVERSE INTERPOLATION *

I	Y(I)		LOWER LIMIT FOR X	PREDICTED X	UPPER LIMIT FOR X
1	3713.000	<	1.705250	1.705890	1.709779
2	3823.000		1.749691	1.753002	1.756223
3	3933.000		1.797422	1.800113	1.802745
4	4043.000		1.844952	1.847225	1.849473
5	4153.000		1.892090	1.894297	1.896511
6	4263.000		1.939002	1.941202	1.943401
7	4373.000		1.985893	1.988067	1.990239
8	4483.000		2.032783	2.034931	2.037077
9	4593.000		2.079673	2.081796	2.083916
10	4703.000		2.126563	2.128660	2.130755
.					
.					
.					
164	21643.00		9.704492	9.706814	9.709139
165	21753.00		9.755669	9.758022	9.760378
166	21863.00		9.806846	9.809230	9.811617
167	21973.00		9.858023	9.860439	9.862857
168	22083.00		9.909199	9.911647	9.914098
169	22193.00		9.960375	9.962855	9.965338
170	22303.00		10.01155	10.01406	10.01656
171	22413.00		10.06267	10.06506	10.06742
172	22523.00		10.11361	10.11578	10.11793
173	22633.00		10.16435	10.16651	10.16866
.					
.					
.					
234	29343.00		13.28631	13.28856	13.29082
235	29453.00		13.33740	13.33971	13.34203
236	29563.00		13.38849	13.39087	13.39325
237	29673.00		13.43957	13.44202	13.44447
238	29783.00		13.49066	13.49317	13.49570
239	29893.00		13.54174	13.54433	13.54692
240	30003.00		13.59281	13.59548	13.59815
241	30113.00	L	13.64334	* .0000000	> 13.64334
242	30223.00	L	13.64334	* .0000000	> 13.64334

*** AT LEAST ONE Y-VALUE IS OUTSIDE THE RANGE ***
 *** OF AT LEAST ONE CALIBRATION CURVE ***

S DENOTES THE VALUE OF THE SMALLEST KNOT

L DENOTES THE VALUE OF THE LARGEST KNOT

* DENOTES VALUES OUTSIDE THE RANGE OF THE CALIBRATION DATA - NO
 VALID PREDICTION IS AVAILABLE

< INDICATES THAT NO VALID LOWER CALIBRATION LIMIT
 GREATER THAN THE MINIMUM POSSIBLE X-VALUE IS AVAILABLE.

> INDICATES THAT NO VALID UPPER CALIBRATION LIMIT
 SMALLER THAN THE MAXIMUM POSSIBLE X-VALUE IS AVAILABLE.

Figure 4. Calibration chart. Y is pressure in pascals; X is volume in M³.

```

*****
* FIXED-KNOT SPLINE PACKAGE FOR CALIBRATION *
*****

```

REAL DATA FROM A TANK CALIBRATION (DATA IN FILE CPR*NS.96)

----- FULL PRINTOUT -----

<<<< EACH END KNOT DUPLICATED 1 TIMES >>>>

 * SUMMARY OF KNOT LOCATIONS *

I	KNOTS(I)
1	1.70525
2	1.70525
3	1.29466
4	4.54674
5	5.49482
6	5.87381
7	6.44156
8	7.13990
9	10.0425
10	10.2320
11	12.5044
12	13.6433
13	13.6433

 * PARAMETERS OF LEAST SQUARES SPLINE FIT *

DEGREE OF SPLINE = 1

NUMBER OF	OBSERVATIONS =	172
NUMBER OF	ZERO WEIGHTS =	0
NUMBER OF	NON-ZERO WEIGHTS =	172
NUMBER OF	KNOTS =	13
NUMBER OF	B-SPLINES =	11

NUMBER OF Y VALUES
 FOR WHICH X CONFIDENCE = 242
 INTERVAL IS TO BE COMPUTED

<<<< 11 B-SPLINE COEFFICIENTS COMPUTED >>>>

Figure 5. Preliminaries.

 * ANALYSIS OF RESIDUALS *

I	WEIGHT W(I)	X(I)	OBSERVED Y(I)	PREDICTED Y(I)	RESIDUAL(I)	STD DEV OF PREDICTED Y(I)
1	1.0000	1.705250	3711.640	3711.505	.13455	1.052565
2	1.0000	1.705270	3711.420	3711.552	-.13223	1.052453
3	1.0000	1.894010	4152.240	4152.238	.18311-02	.4110981
4	1.0000	1.894140	4152.130	4152.542	-.41168	.4113765
5	1.0000	1.894580	4151.050	4153.569	-2.5190	.4123280
6	1.0000	1.894650	4151.910	4153.732	-1.8225	.4124807
7	1.0000	1.894660	4153.400	4153.756	-.35577	.4125026
8	1.0000	2.084060	4599.320	4598.315	1.0054	.3729185
9	1.0000	2.084110	4600.090	4598.432	1.6581	.3729083
10	1.0000	2.272720	5044.100	5041.136	2.9636	.3359134
11	1.0000	2.273020	5042.730	5041.841	.88947	.3358569
162	1.0000	13.07486	28884.68	28883.46	1.2214	.2921614
163	1.0000	13.26022	29282.92	29282.06	.86230	.3425575
164	1.0000	13.26158	29285.71	29284.98	.72754	.3430482
165	1.0000	13.26232	29284.50	29286.57	-2.0735	.3433159
166	1.0000	13.45198	29695.29	29694.42	.87061	.4235761
167	1.0000	13.45385	29699.14	29698.44	.69897	.4244610
168	1.0000	13.63914	30096.50	30096.89	-.38940	.5180907
169	1.0000	13.64052	30099.62	30099.86	-.23706	.5188241
170	1.0000	13.64133	30098.26	30101.60	-3.3391	.5192548
171	1.0000	13.64143	30102.36	30101.81	.54614	.5193080
172	1.0000	13.64333	30105.91	30105.90	.10254-01	.5203189

RESIDUAL STD DEV
1.48848

RESIDUAL D.F.
161

 * ESTIMATION OF B-SPLINE COEFFICIENTS *

I	B-SPLINE COEF	STD DEV
1	3711.5053	1.0525651
2	4153.7559	.41250259
3	10378.705	.41074148
4	12579.214	.57466792
5	13403.155	.74306913
6	14630.321	.62254084
7	16236.443	.41161732
8	22364.034	.44698178
9	22774.945	.43252287
10	27656.846	.39959609
11	30105.922	.52032419

<<<< GRID OF 300 EVENLY SPACED X VALUES CREATED >>>>

<<<< STD. DEV. OF 300 PREDICTED Y VALUES COMPUTED >>>>

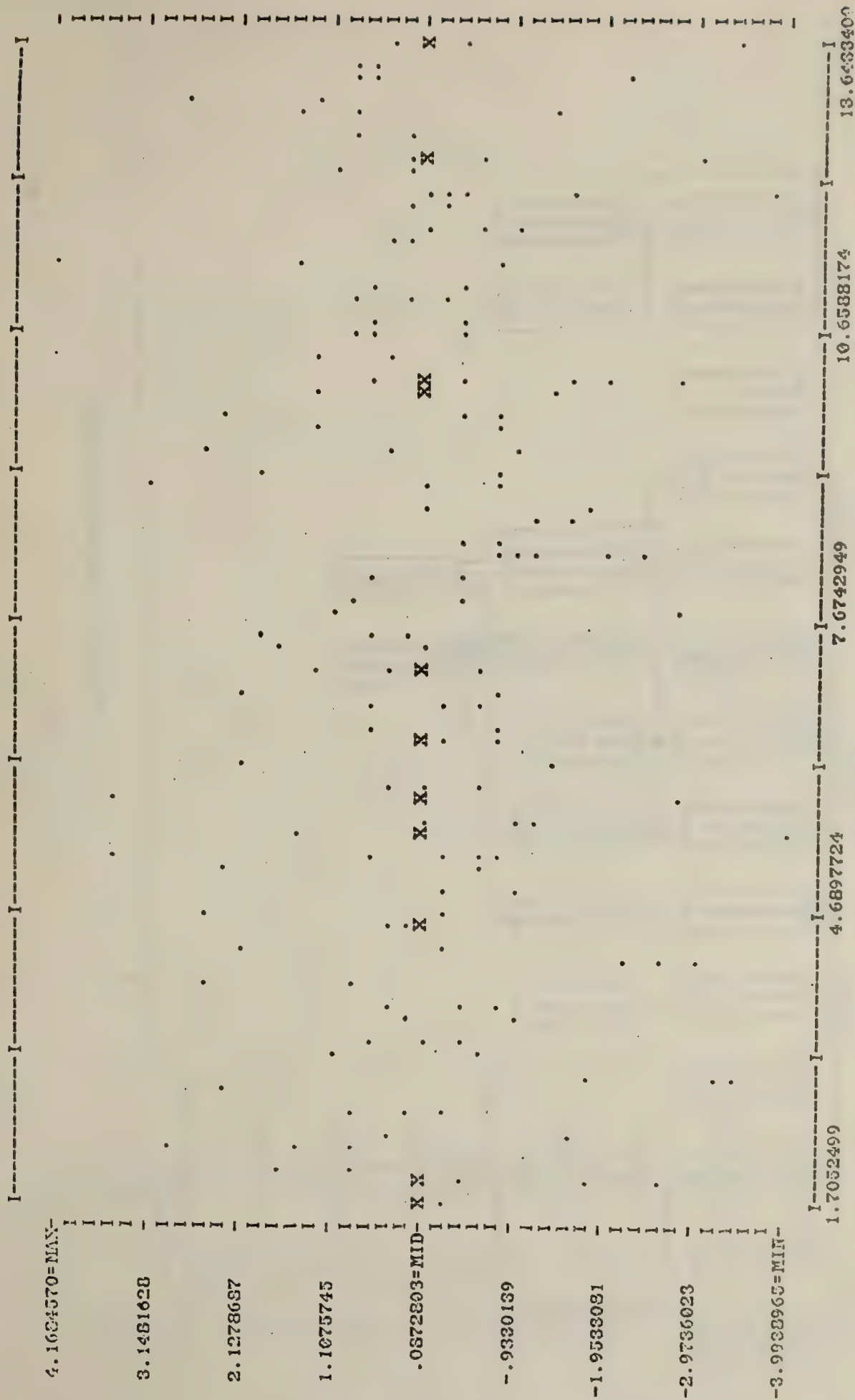
Figure 6. Regression fit.

 * PIECEWISE POLYNOMIAL REPRESENTATION OF SPLINES *

.....INTERVAL.....			COEFFICIENTS OF (X-X(I))**P	
I	X(I)	X(I+1)	P = 0	1
1	1.7052	1.8947	3711.5	2334.9
2	1.8947	4.5467	4152.8	2347.2
3	4.5467	5.4948	10379.	2321.0
4	5.4948	5.8738	12579.	2174.0
5	5.8738	6.4416	13403.	2161.5
6	6.4416	7.1899	14639.	2146.2
7	7.1899	10.043	16236.	2148.1
8	10.043	10.232	22364.	2168.6
9	10.232	12.504	22775.	2148.3
10	12.504	13.643	27657.	2150.4

Figure 7. Ordinary polynomial
 representation of the fitted spline.

Residuals (pascals) vs. independent variable (m^3).



KNOT LOCATIONS ARE INDICATED BY THE SYMBOL X

Figure 8. Residual plot.

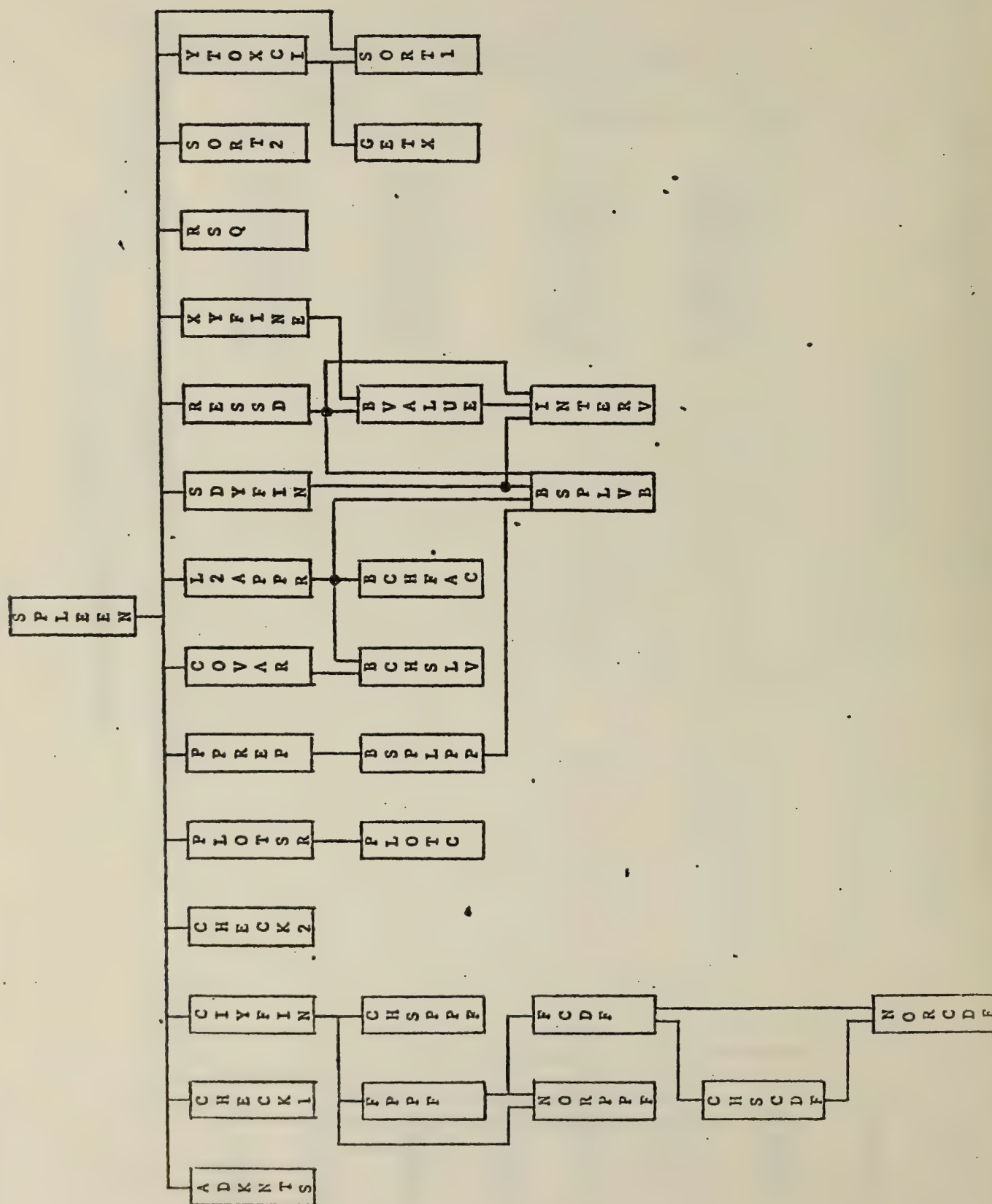
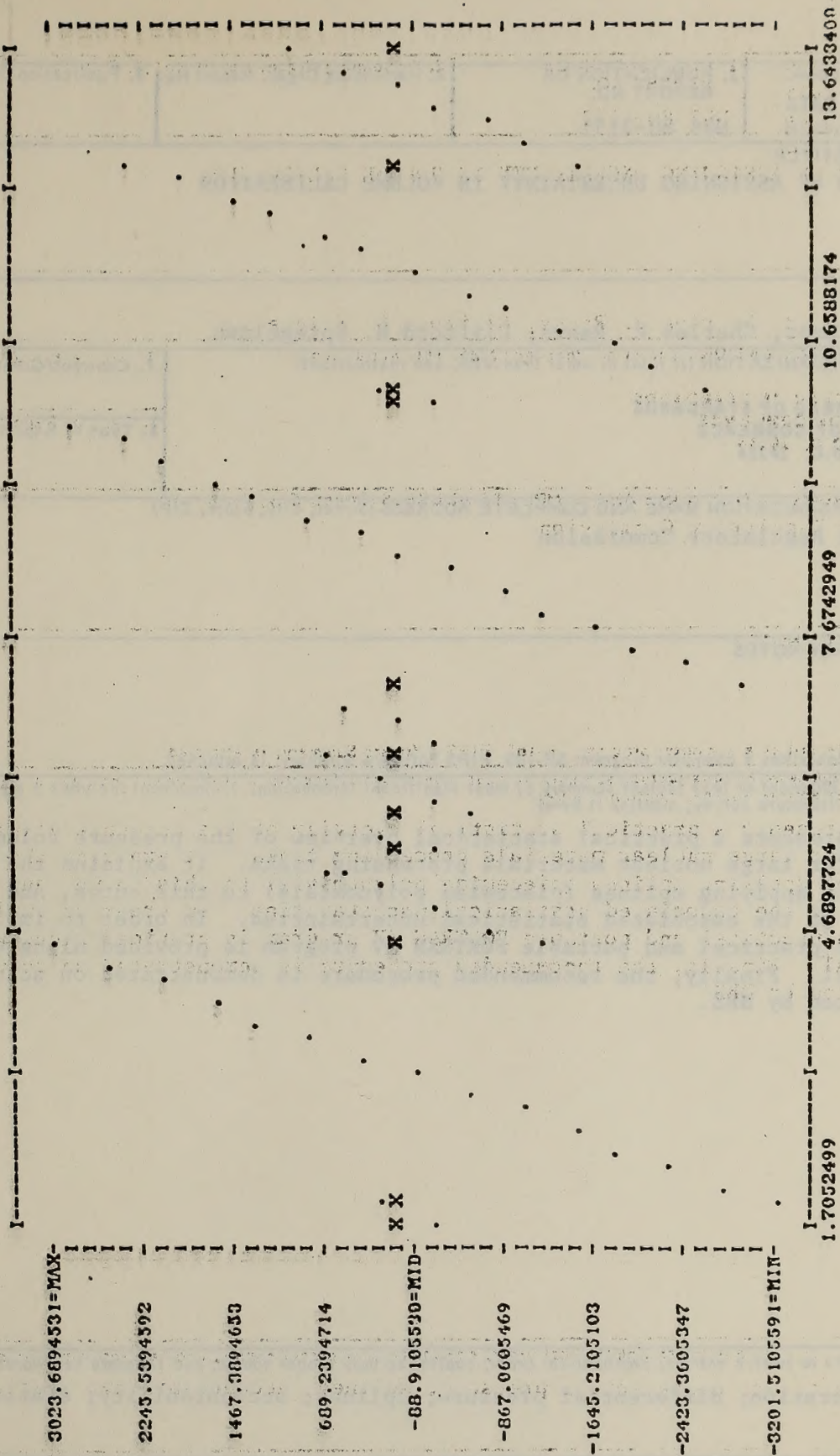


Figure 9. Diagram of subroutine interactions.

RESIDUALS VS. INDEPENDENT VARIABLE



KNOT LOCATIONS ARE INDICATED BY THE SYMBOL X

Figure 10: Diagnostic plot of residuals from a zero-degree spline fit (i.e., a step function).

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12. KEY WORDS (Six to twelve entries; alphabetical order; capitalize only proper names; and separate key words by semicolons) Volume calibration; differential pressure; splines; accountability; statistics.			
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